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INSTRUCTION AND MAINTENANCE MANUAL for RETURN LOSS MEASURING SETS

KS-20501 L3-Issue 3

KS-20501 L4-Issue 3

BOWMAR

BOWMAR / ALI, Inc.

A SUBSIDIARY OF BOWMAR INSTRUMENT CORPORATION

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INSTRUCTION AND MAINTENANCE MANUAL for RETURN LOSS MEASURING SETS

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KS-20501 L4-Issue 3

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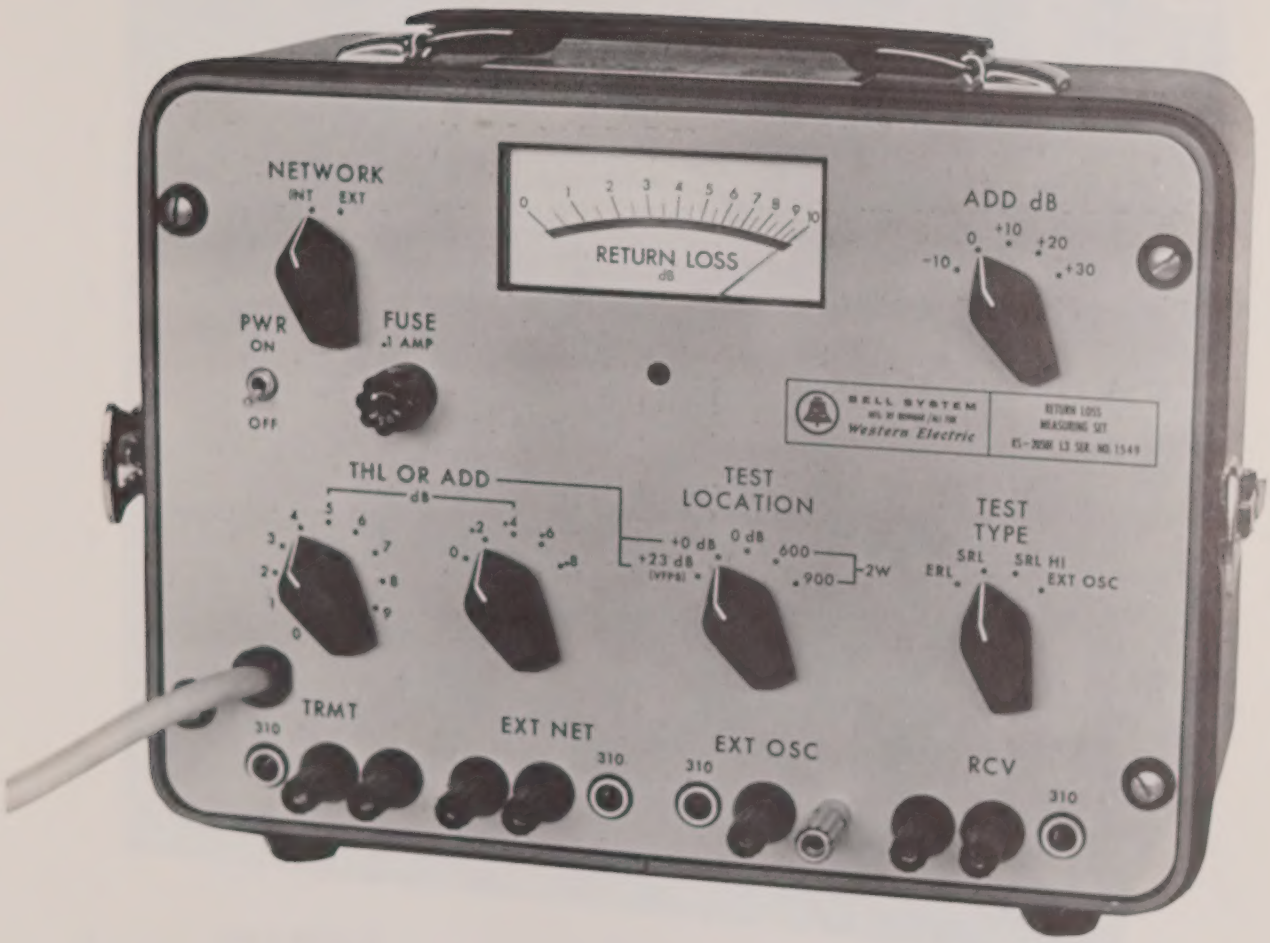
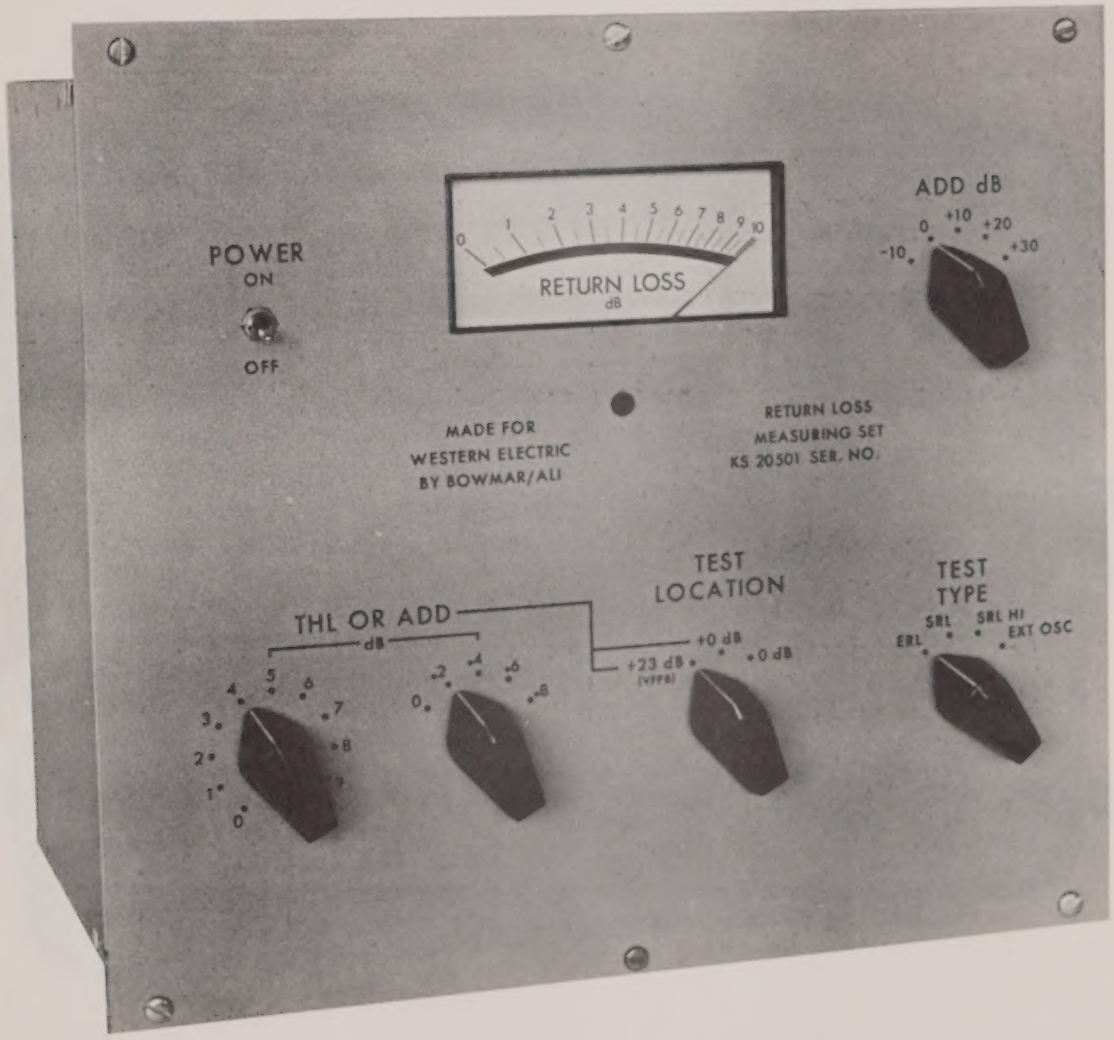


RETURN LOSS MEASURING SET
KS-20501 L3



RETURN LOSS MEASURING SET
KS-20501 L4

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1.0 INTRODUCTION

1.1 Description

The KS-20501 Return Loss Measuring Set is an instrument designed to make those measurements , for through and terminal balance in central offices, which are required to control speech echoes and prevent singing or oscillating conditions.

1.2 Scope of Manual

This manual describes the various modes of return loss measurement. It contains detailed instructions for operation, routine maintenance, and calibration, as well as trouble shooting and minor repair procedures. Schematic diagrams with typical voltages and waveforms are included, supplemented by component and path locating diagrams. A parts list, with the names and addresses of manufacturers is also included.

1.3 Designation of Instruments

The KS-20501 L3 model of the Return Loss Measuring Set is a portable unit operated from a 115 V 60 Hz line. It is designed to make 2-wire and 4-wire return loss measurements.

The KS-20501 L4 model of the Return Loss Measuring Set is a rack-mounted unit powered from a remote -48 V dc source and is designed to make 4-wire return loss measurements only.

1.4 Specification Summary

Test Type:	Echo Return Loss (ERL) Singing Return Loss (SRL) Singing Return Loss High Frequency (SRL HI) Single Frequency Return Loss (External Oscillator)
Modes:	2-wire, 600 and 900 ohms, L1 only 4-XB Test Hybrid VFPB
Filter Characteristics (-3 dB points):	ERL: 560 to 1965 Hz SRL: 260 to 500 Hz SRL-HI: 2200 to 3400 Hz

External Oscillator Range: 200 Hz to 15 kHz

Impedances:
2-wire: 600 and 900 ohms, L3 only
4-wire: 600 ohms
EXT OSC Input: 600 ohms

Return Loss Range: -10 dB to +40 dB

Accuracy: ±0.4 dB, all test types

Internal Hybrid Balance Network:
2.16 μF in series with 600 or 900 ohms, L3 only

4-Wire Circuit Loss Compensation:
+23 dB (VFPB): 23 dB of fixed gain inserted plus 10 dB adjustable in 0.2 dB steps
+0 dB: 10.8 dB adjustable in 0.2 dB steps
0 dB: 0 dB internal gain

Output Signal: Type: weighted white noise, with provisions for external oscillator

Output Level:
2-wire: -8 dBm for 600 ohms
-9.8 dBm for 900 ohms
4-wire: -2 dBm for 600 ohms

Longitudinal Balance: 70 dB at 100 Hz and 55 dB at 3 kHz

Fault Voltages:
(a) Any line input will withstand 600 Vdc to ground.
(b) All specifications are met when input line carries nominal 48 V. Unit will not be damaged by 105 V rms 20 Hz ringing signal for 10 seconds.

Primary Power:
L3: 117 Vac ±10%, 60 Hz
L4: -48 Vdc ±4 V

Size and Weight:
L3: 8-3/4" H x 12" W x 7-5/8"D
Approximately 15 lb. with cover
L4: 10"H x 11"W x 6-1/4"D
Approximately 12 lb.

Operating Temperature and Humidity:
0 to 50°C, 95% relative humidity

1.5 General Background Information

The general principle used in making return loss measurements is diagrammed in the hybrid 4-port network, as shown in FIG. 1-A.

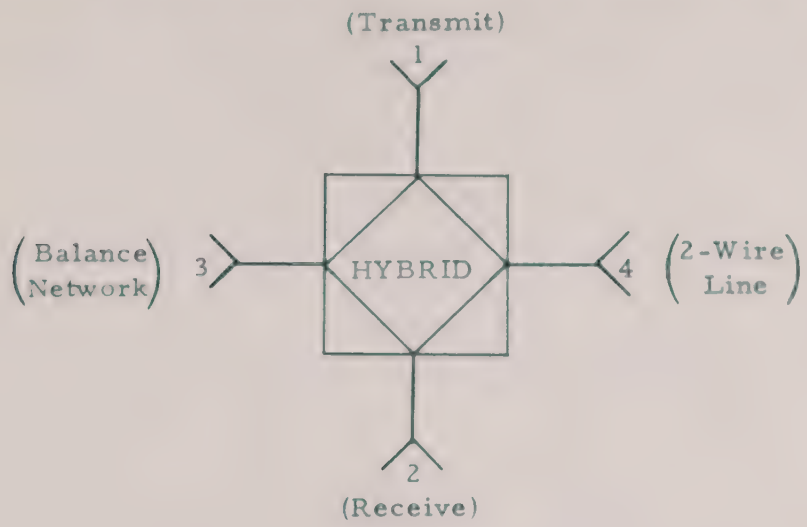


FIG. 1-A

The impedance of port 1 must equal that of port 2, and the impedance of port 3 must equal that of port 4, for the hybrid to be perfectly balanced. The attenuation from ports 1 to 4 and ports 4 to 2 is 3 dB for a transformer type hybrid and 6 dB for a resistive type hybrid.

Where α_{1-4} is the attenuation from port 1 to port 4, α_4 is the return loss of port 4, and α_{4-2} is the attenuation from port 4 to port 2, the total attenuation from port 1 to port 2 is described as in the following equation:

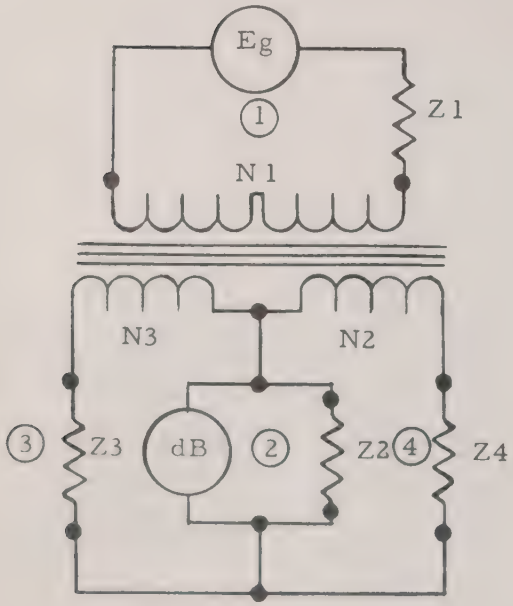
$$\alpha_{1-2}=\alpha_{1-4}+\alpha_4+\alpha_{4-2}$$

When the impedance of port 4 (2-Wire Line) does not match the impedance of port 3 (Balance Network) the attenuation from port 1 to port 2 is the return loss of port 4 plus the total attenuation from ports 1 to 4 and 4 to 2.

A return loss measurement of the impedance at port 4 can be made with a signal generator of proper impedance connected to port 1 and a dB meter of equal impedance connected to port 2. In the case of the transformer hybrid, with a known balancing network at port 3, the return loss of the unknown at port 4 is determined by measuring the signal attenuation from port 1 to port 2 and subtracting 6 dB. For example, the return loss of the network at port 4, with respect to the balancing network at

port 3, is 36 dB if the loss from port 1 to port 2 is 42 dB. It should be noted that all four port impedances must be equal in the balanced condition when using a resistive hybrid for return loss measurement. A transformer hybrid must be used when the impedances of ports 1 and 2 are not equal to ports 3 and 4. Examples of resistive and transformer hybrids are shown in FIG. 1-B and FIG. 1-C.

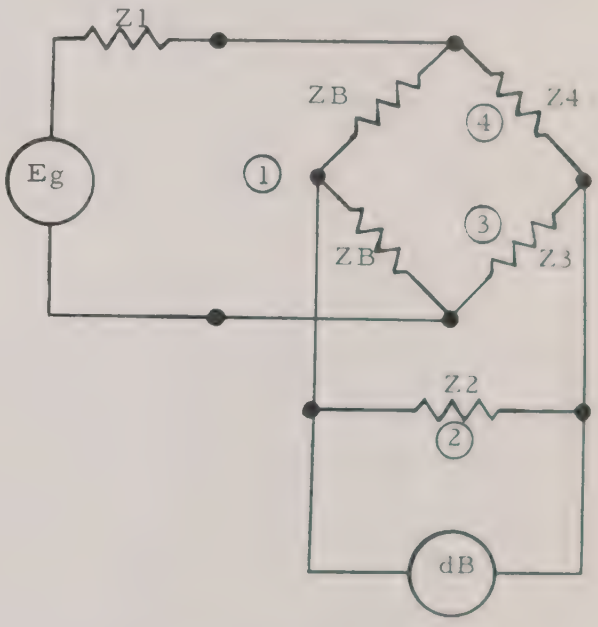
Z2= Z3 N 2= N3



TRANSFORMER HYBRID

FIG. 1-B

Z1= Z2= ZB= Z4



RESISTIVE HYBRID

FIG. 1-C

The return loss measurement can initially be calibrated to 0 dB return loss by open- or short-circuiting the terminals at port 4; then, when the unknown load is connected to port 4, absolute value of the new dB meter reading will be the return loss. This method of calibration is valid only if the generator and dB meter impedances are matched to the hybrid.

A method of performing ERL, SRL, AND SRL HI functions for 2-wire measurements in one unit is shown in the block diagram in FIG. 1-D.

A diode noise source provides a flat spectrum between 200 Hz and 4 kHz. Three band pass filters shape the noise spectrum to be used in the measurement. ERL (560 to 1965 Hz), SRL (260 to 500 Hz), and SRL HI (2200 to 3400 Hz) are used for measurement. The use of an external oscillator for determining exact frequency of minimum return loss is also shown.

The band limited noise signal is passed through a resistive hybrid network which uses the 2-wire line and compromise network. The null signal of the hybrid bridge, which is a measure of the return loss of 2-wire line, is passed through a meter attenuator and amplifier to the return loss meter. The meter is calibrated in dB and the total return loss is read by adding the meter indication to the attenuator switch indication.

The noise generator enables a measurement of return loss of a complete frequency spectrum at one time while the external oscillator capability provides for measuring return loss at specific frequencies.

The same basic circuitry that is shown in FIG. 1-D can be used to make balance measurements on external 4-wire terminating sets. Balance measurements are made using the 4-wire mode. The configuration for these 4-wire measurements is shown in FIG. 1-E, where the hybrid is omitted and the test set is used as both a noise generator and a level measuring set. The band limited noise signal is passed through the transmitting 4-wire line to the 4-wire terminating set. The amount of signal returned on the receiving 4-wire line is in measure of the balance of the 4-wire terminating sets. Corrections for normal attenuation in the 4-wire line can be made by a Trans Hybrid Loss (THL) amplifier which is adjustable in 0.2 dB steps from 0 to 10.8 dB. When the test is being made through a Voice Frequency Patch Bay (VFPB), an additional fixed 23 dB of gain can be inserted to compensate for the added loss.

1.6 Standard Filter Curves

Three line-graphs that represent standard filter curve characteristics are shown on pages 1-8, 1-9, and 1-10. These curves show relative attenuation in dB versus frequency in Hz for the ERL (Echo Return Loss), SRL (Singing Return Loss), and SRL HI (Singing Return Loss High Frequency) filters.

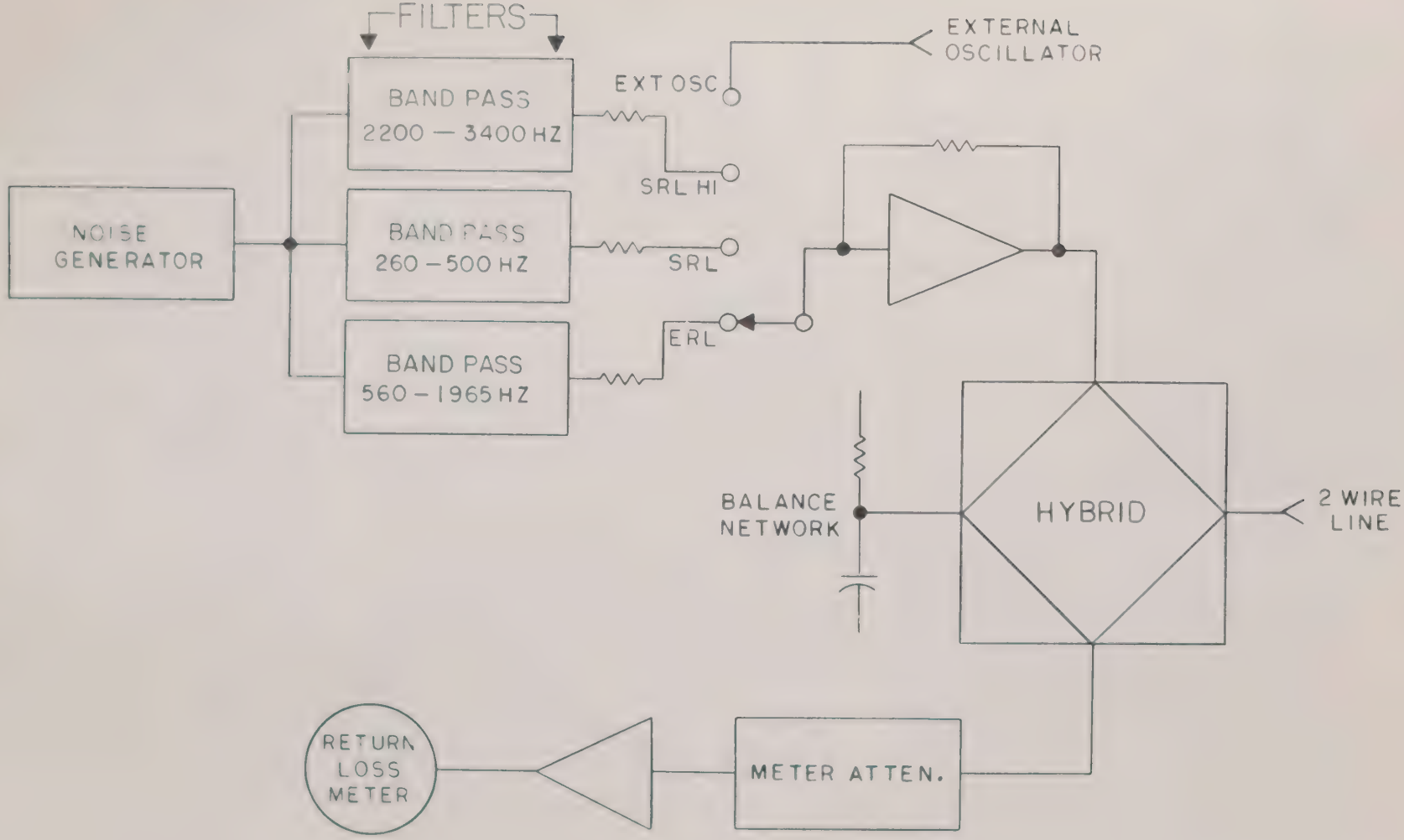


FIG. 1-D

2-WIRE LINE MEASUREMENTS

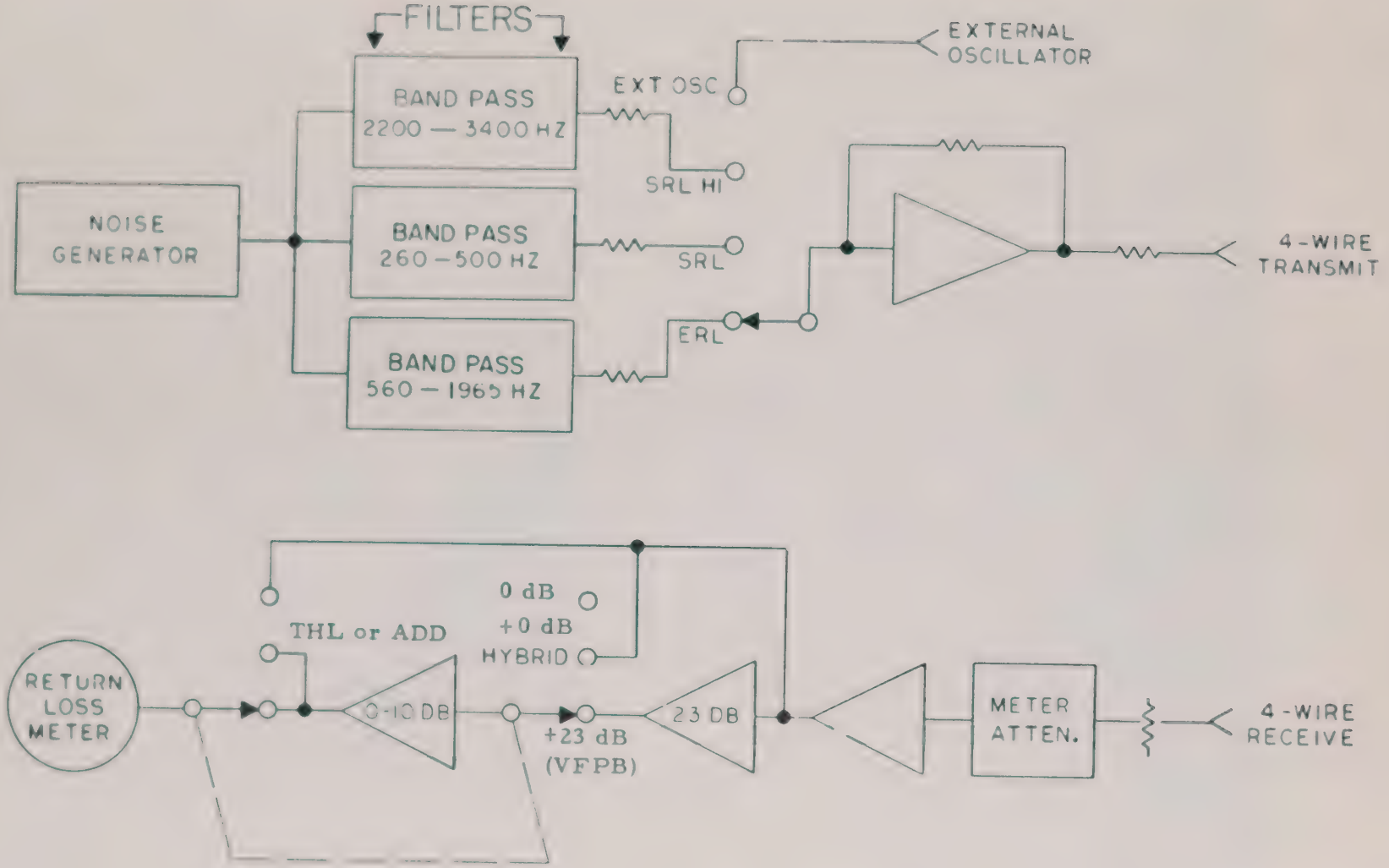


FIG. 1-E

4-WIRE LINE MEASUREMENTS

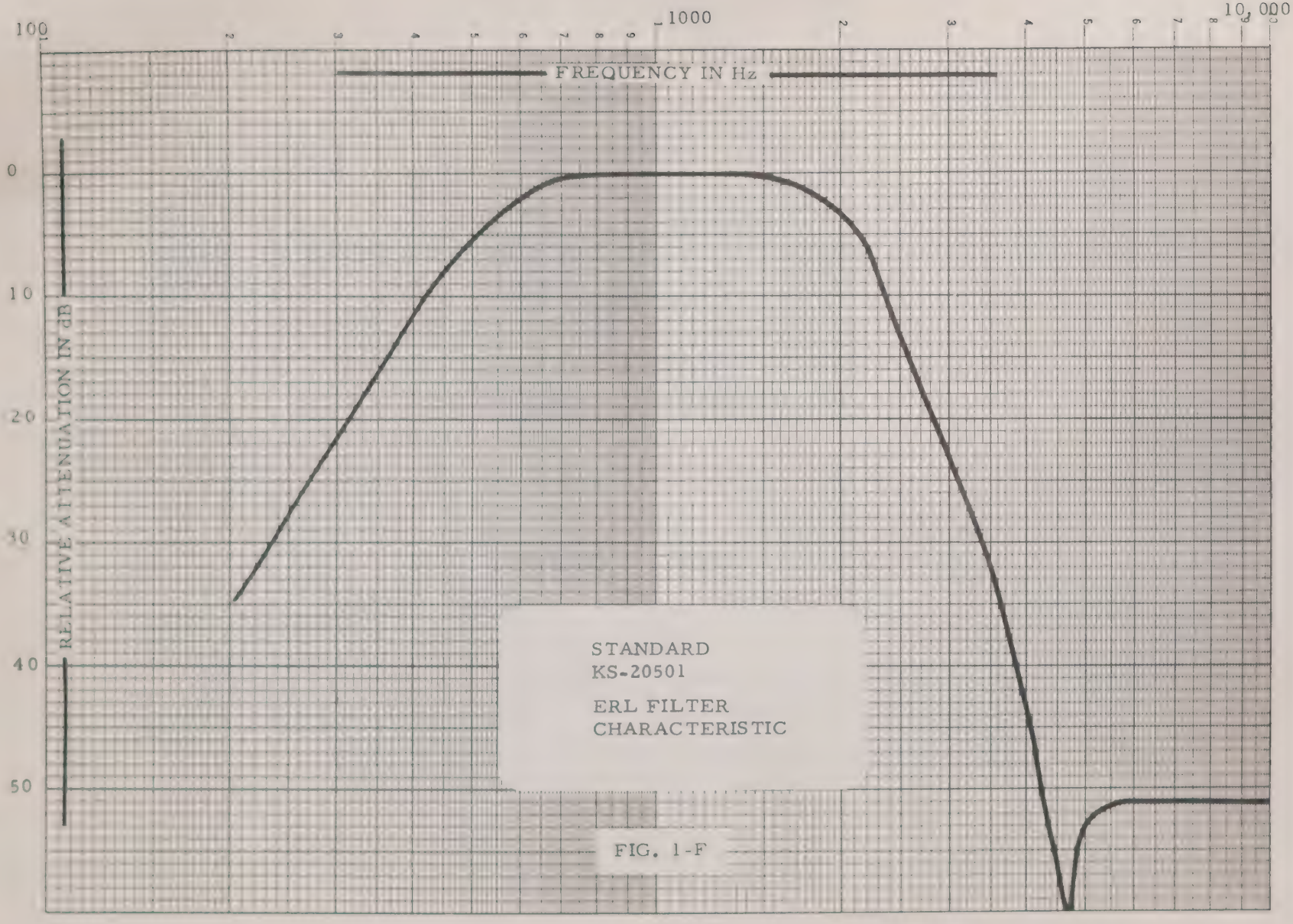

100
1000
10,000
FREQUENCY IN Hz
0
10
20
30
40
50
RELATIVE ATTENUATION IN dB
STANDARD
KS-20501
ERL FILTER
CHARACTERISTIC

FIG. 1-F

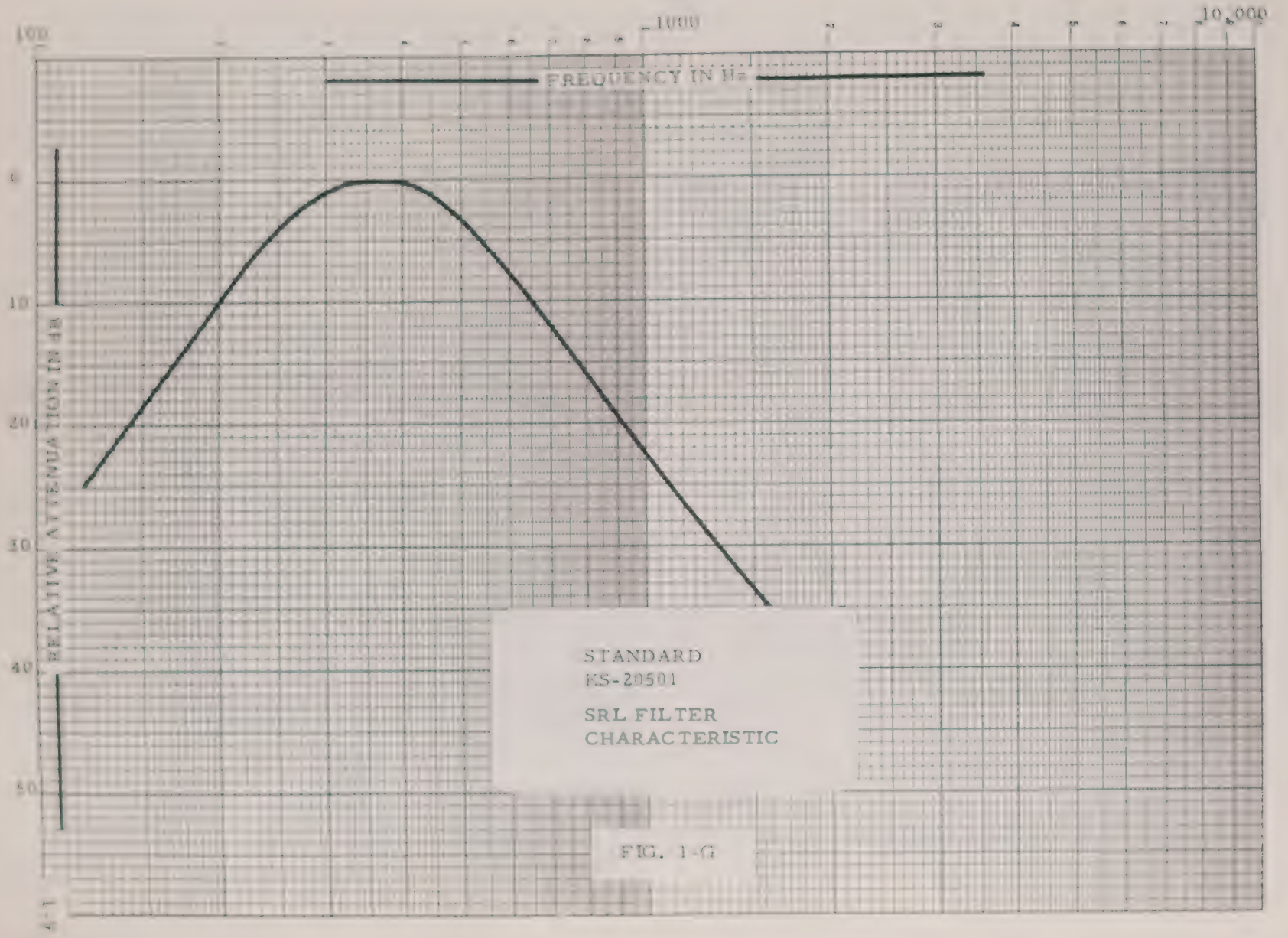

100
1000
10,000
FREQUENCY IN Hz
0
10
20
30
40
50
RELATIVE ATTENUATION IN dB
STANDARD
FS-20501
SRL FILTER
CHARACTERISTIC

FIG. 1-G

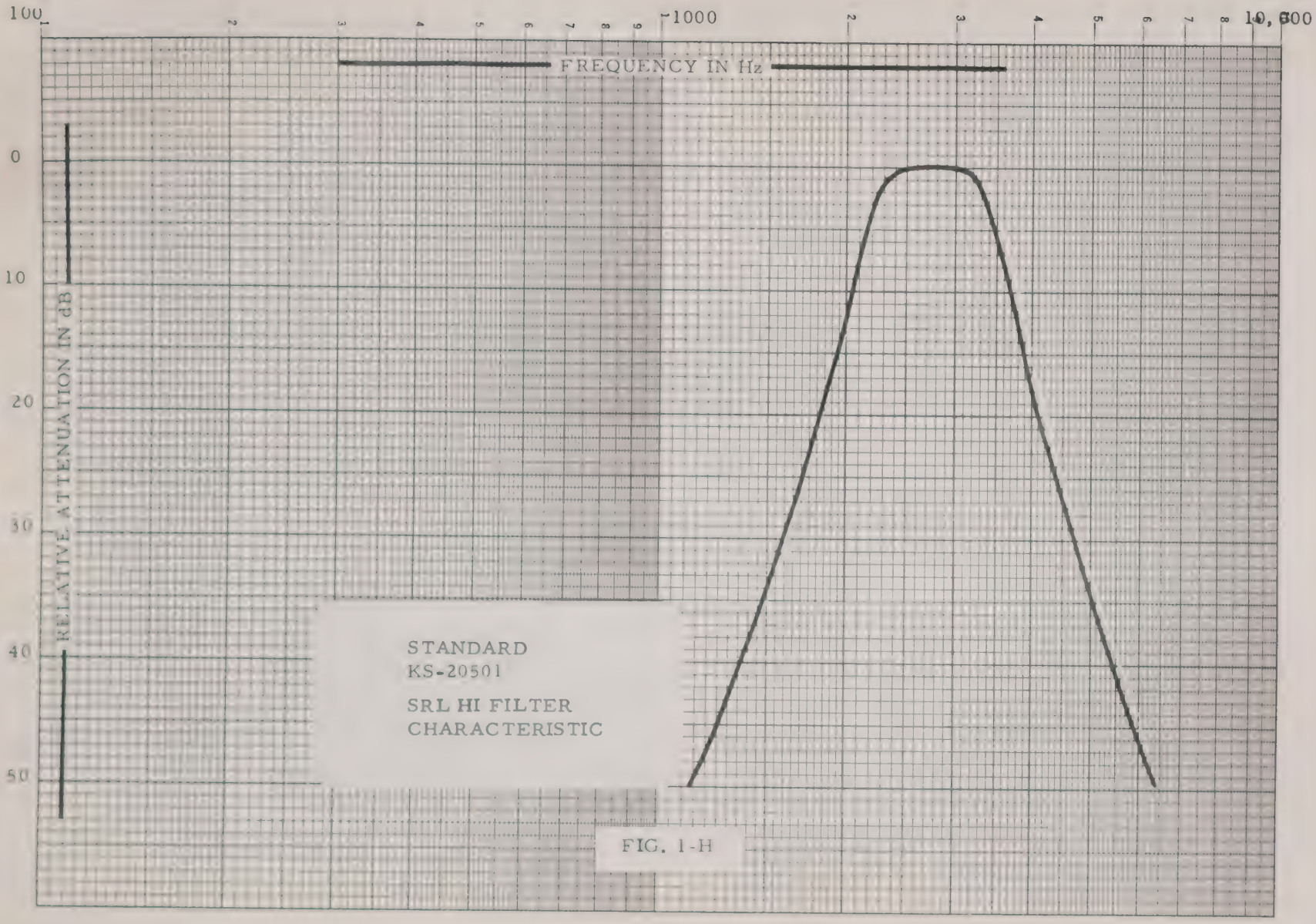

100
1000
10,000
FREQUENCY IN Hz
RELATIVE ATTENUATION IN dB
0
10
20
30
40
50
STANDARD
KS-20501
SRL HI FILTER
CHARACTERISTIC

FIG. 1-H

2.0 OPERATING INSTRUCTIONS

2.1 Controls, Jacks, and Meter

.1 TEST TYPE

This four-position switch allows selection of three internally generated signals or an externally connected oscillator test signal. The positions are designated ERL (Echo Return Loss), SRL (Singing Return Loss), SRL HI (Singing Return Loss High Frequency), and EXT OSC (External Oscillator).

.2 TEST LOCATION

On the KS-20501 L this control is a five-position switch to select the sensitivity and measurement configuration of the set. The positions are designated +23 dB, +0 dB, 0 dB, 600, 900 (2-wire measurement). The KS-20501 L4 has the control as above, but without the 600, 900 (2-wire measurement) positions.

.3 NETWORK

This control is on the KS-20501 L3 set only, and is a two-position switch which selects between internal and external networks for 2-wire measurements. (Refer to Circuit Descriptions, Para. 3.2.7.) The positions are designated INT and EXT.

.4 THL OR ADD

These two rotary switches are used to adjust the sensitivity of both KS-20501 L3 and L4 sets to allow for losses in the measured circuit, which should not be included in the return loss measurement. One is a ten-position rotary switch which is marked from 0 dB to 10 dB in 1 dB increments, and the second is a five-position rotary switch in series with the first, marked from 0 dB to .8 dB in 0.2 dB increments. These two controls are bracketed with a dB indication and headed by the total THL OR ADD designation. A line running from THL OR ADD to +0 dB and +23 dB indicates their effect in these two TEST LOCATION positions.

.5 ADD dB

This five-position rotary switch is used in both the KS-20501 L3 and L4 sets to select signal level to the detector circuit to maintain the meter on-scale. The positions are designated -10, 0, +10, +20, +30, and when added to the meter indication it results in the return loss measurement. Negative numbers indicate return gain.

.6 PWR

This two-position toggle switch is used to connect and disconnect power to the circuits of both the KS-20501 L3 and L4 sets. The positions are designated ON, OFF.

.7 TRMT

These three jacks on the KS-20501 L3 provide access to the output test signal in the 4-W mode and are also used to connect the line under test in the 2-W mode. One jack accepts a WECO 310-type plug and is designated 310; the other two consist of black binding posts paired to accept a General Radio 938-type plug (or equivalent). One binding post is connected to the tip terminal of the 310 jack; the other is connected to the ring terminal of the 310 jack. The sleeve terminal of the TRMT jack is connected to the sleeve terminal of RCV jack. The KS-20501 L4 has rear terminal access to the output test signal.

.8 RCV

These three jacks on the KS-20501 L3 provide access for receiving the test signal from a 4-wire connection. One jack accepts a WECO 310-type plug and is designated 310; the other two consist of black binding posts paired to accept a General Radio 938-type plug (or equivalent). One binding post is connected to the tip terminal of the 310 jack; the other is connected to the ring terminal of the 310 jack. The sleeve terminal of the RCV jack is connected to the sleeve terminal of the TRMT jack. The KS-20501 L4 has rear terminal access for receiving the test signal.

.9 EXT OSC

These three jacks on the KS-20501 L3 provide access for using an external oscillator when measuring point-by-point return loss. One jack accepts a WECO 310-type plug and is designated 310; the other two consist of binding posts paired to accept a General Radio 938-type plug (or equivalent). The black binding post is connected to the tip terminal of the 310 jack; the natural metal binding post connects to the ring terminal and ground. There is no connection to the sleeve. These jacks are connected to the measuring portion of the set only when the TEST TYPE control is in the EXT OSC position. The KS-20501 L4 has rear terminal access to an external oscillator.

.10 EXT NET

These three jacks, on the KS-20501 L3 only, provide access for external network substitution when making 2-Wire measurements. One jack accepts a WECO 310-type plug and is designated 310; the other two consist of black binding posts paired to accept a General Radio 938-type plug (or equivalent). One binding post is connected to the tip terminal of the 310 jack; the other binding post is connected to the ring terminal of the 310 jack. The sleeve terminal has no connection. These jacks are connected to the measuring portion of the set when the NETWORK control is in either the EXT or INT position.

.11 RETURN LOSS dB

This meter is a linear movement, with a logarithmic electrically expanded scale of 0 to 10 dB in 0.5 dB increments and indicates an increasing return loss with an up-scale reading. It measures the total return loss when used in conjunction with the ADD dB control.

2.2 Procedures

.1 TEST LOCATION Selection

The first step in making a return loss measurement is a proper setting for the TEST LOCATION control selected from the following:

+23 dB - Used when testing at a voice frequency patch bay; provides a fixed 23 dB gain to compensate for the level difference plus an additional 10.8 dB of gain adjustable in 0.2 dB steps (THL) to compensate for line loss.

+0 dB - used when testing 4-wire terminating sets; allows for 10.8 dB gain, adjustable in 0.2 dB steps using the THL controls, to compensate for line and trans-hybrid loss.

0 dB - used when testing 4 wire circuits where no line loss compensation is necessary.

600-900 - used in 2-wire measurements.

.2 TEST TYPE Selection

The second step in making a return loss measurement is to determine the type of signal that will be used to stimulate the 2-wire or 4-wire line. The selection of the signal is accomplished by positioning the TEST TYPE control, on the front panel of the test set, to one of the following:

ERL - provides gaussian noise through a filter with 3 dB bandwidths of 560 to 1965 Hz.

SRL - provides gaussian noise through a filter with 3 dB bandwidths of 260 to 500 Hz.

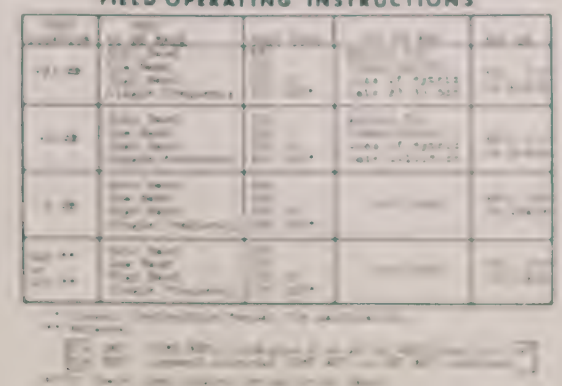
SRL HI - provides gaussian noise through a filter with 3 dB bandwidths of 2200 to 3400 Hz.

EXT OSC - allows for the use of an external oscillator with the signal injected at the EXT OSC terminals. Any signal with a frequency of 200 Hz to 15 kHz may be used. In this mode of operation, the AGC loop is not in effect; therefore, the output level of the transmitter must be controlled by the external oscillator.

NOTE The approximate level for the external oscillator should be -3 dBm into 600 ohms, or about 0.55 V rms into the EXT OSC terminals.

.3 The following are the operating instructions as found in the cover of the portable test set.

RETURN LOSS TEST SET
FIELD OPERATING INSTRUCTIONS



2. 2. 4 2-Wire Return Loss Measurements

Set the TEST LOCATION control to either the 600 or 900 2-wire position as required. Select the desired signal using the TEST TYPE control. If the internal balancing network is to be used, the NETWORK control must be in its INT position; if an external network is to be used, the NETWORK control must be in its EXT position and a suitable network connected across the EXT NET terminals. The 2-wire line or unknown network to be measured is connected to the TRMT terminals. The ADD dB control is adjusted until the RETURN LOSS meter provides an on-scale indication. The indication of the RETURN LOSS meter in dB is added to the dB setting of the ADD dB control to give the total return loss.

Calibration is necessary with this test set only when the TEST TYPE control is in the EXT OSC position. Set TEST TYPE control in the EXT OSC position; the TEST LOCATION control in either 2-wire position; the NETWORK control in the INT position; no connection made to the TRMT terminals; the ADD dB control in the 0 position; adjust the external oscillator level control for a 0 dB indication on the RETURN LOSS meter. After this calibration is performed, any 2-wire measurement may be made as long as the external oscillator level remains constant. See 2. 2. 2 for external oscillator level.

. 5 4-Wire Measurements

Select the desired signal using the TEST TYPE control.

The transmitting 4-wire line is connected to the TRMT terminals and the receiving 4-wire line is connected to the RCV terminals. If the +23 dB or +0 dB positions of the TEST LOCATION control are used, the known line loss correction should be inserted by adjusting the THL controls. Adjust the ADD dB control until an on-scale indication is obtained on the RETURN LOSS meter. The return loss is read directly by adding the meter dB indication to the ADD dB control indication.

As in the 2-wire mode, no prior calibration is necessary with this test set except when used in the EXT OSC position of the TEST TYPE control.

If an external oscillator is used, the calibration procedure for 4-wire measurements is as follows: with the TEST TYPE control set to the EXT OSC position; the external oscillator connected to the EXT OSC terminals; the TEST LOCATION control in the 0 dB position; the ADD dB control in the 0 position. Loop the TRMT terminals to the RCV terminals with a cable and adjust the external oscillator output level control for a RETURN LOSS meter indication of 0 dB. After this calibration is performed, any 4-wire measurement may be made as long as the external oscillator level remains constant. See 2. 2. 2 for external oscillator level.

2.3 Signal and Power Connections

.1 KS 20501 L3 Connections

Use connections as labelled on the front panel.

.2 KS 20501 L4 Connections

Pin designations are:

Signal	Pin No.
RCV	1 and 5
TRMT	4 and 8
Ground	6 and 7
-48V DC Input	2
Ext. Osc. Input	3

On the rear panel, a jack (J1 26-440-8P Amphenol) will receive a plug (P1 26-4501-8S Amphenol) which is furnished with the unit.

3. 0 CIRCUIT DESCRIPTION

3. 1 General

The list 3 and list 4 sets may be divided into two major sections - Transmitter and Receiver. The block diagrams (Fig. 3-A and Fig. 3-B) show the circuit functions which are described below. Both sets use the output of a broadband noise generator which is filtered in the transmitter section to provide the test signal. The output level is carefully regulated with an automatic gain control (AGC) loop. The receiver section of the block diagram shows the various gain controlling functions and the final detector and meter which provide a direct reading of return loss.

3. 2 Transmitter

. 1 Noise Generator (see page 6.2.12)

The white noise signal (dc to 300 kHz) voltage which is required to drive the shaping filters is produced by a Zener diode operating on the knee of its breakdown curve. This diode CR5 is biased between the ±12 volt supplies by resistors R89, R90, and R91. Capacitors C40 and C41 are used to decouple power supply ripple from the Zener diode. The output noise signal from the diode is coupled through capacitor C39 to the following stage.

. 2 AGC Amplifier (6. 2. 12)

Integrated circuit amplifier A6 is driven directly from the output of the white noise source and is used to compensate for level variations. Amplifier A6 has a gain of approximately +30 dB to -60 dB and is operated at a nominal gain of 0 dB. The dc control input to A6 on terminal 2 ranges from 0 V dc to -6 V dc. At 0 V dc, A6 is operated at full gain and at -6 V dc it has maximum attenuation. The nominal operating dc voltage at terminal 2 is -3. 3 V. Resistors R83, R84, R85, and R86 are used as voltage dividers to reduce the ±12 V supplies to the ±6 V nominal operating voltages for A6. Capacitors C37 and C38 are used as decoupling capacitors at the power supply inputs to A6. Resistors R95 and R97 are used to bias the inverting and non-inverting inputs to A6. Capacitor C36 is used to couple the output of A6 to the following stage. Amplifier A6 has a flat frequency response from 100 Hz to 1 MHz. The AGC circuit is in effect only when the internal filters are used. When the TEST TYPE switch is in the EXT OSC position, the feedback loop is broken and the output level stability of the transmitter is controlled by the external oscillator used.

. 3 30 dB Wide Band Amplifier (6. 2. 12)

Integrated circuit operational amplifier A5 is used as a wide band (dc to 50 kHz) amplifier with approximately 30 dB of gain. Resistors R38, R39, R41, and R45 are used as a voltage divider to provide feedback from the output of A5 to its inverting input at terminal 3 to establish a gain of 25 dB. R46 is used to bias the non-inverting input terminal 4. Resistors R40, R42, and capacitors C18, C19, are used as frequency compensation networks. Resistors R43, R44, and capacitors C17, C20 are used as decoupling networks to the power supply inputs of A5.

3.2.4 Filters (6.2.5)

The three filters whose 3 dB bandwidths are 260 Hz to 500 Hz, 560 Hz to 1965 Hz, and 2200 Hz to 3400 Hz are made up of similar active circuits using only resistors and capacitors but no inductors. The input to the filters is a common line which is driven from the virtually zero ohm impedance of the 25 dB wide band amplifier.

260-500 Hz Filter: This band pass filter is made up of a separate low pass filter and high pass filter. The high pass section consists of a two-pole stage composed of capacitors C300, C301, resistors R300, R301, and transistors Q300, Q301. The active circuit, made up of transistors Q300 and Q301 is representative of the active circuits used throughout the three filters and will be described at this point.

Transistors Q300 and Q301 operate as a series-shunt feedback amplifier with unity gain high input impedance and low output impedance. Resistor R304 is used to establish the total dc current flowing through Q300 and Q301. Resistor R303 is used to establish the collector current of Q300. The base of Q300 is biased to ground through R302 and R301. R302 is used to suppress parasitic oscillations. Capacitor C303 is used to suppress closed loop oscillations. All the rest of the active circuits operate in the same fashion with the exception that the NPN and PNP transistors are interchanged so that the dc bias level may be maintained at approximately ground potential throughout the filters. The second stage of this high pass filter section is composed of capacitor C304 and resistor R305 (single pole) and transistors Q302 and Q303, therefore the total number of poles for this high pass section is three. The low pass portion of this filter is a two-pole stage of resistors R309, R310, with capacitors C306, C307, and transistors Q304, Q305. The single pole stage is made up of resistor R314 and capacitor C309 with transistors Q306 and Q307. Capacitor C350 is used to block dc from the output. Resistor

560-1965 Hz Filter: This filter is composed of high and low pass sections.

The high pass portion includes two stages. The first is a two pole stage made up of C311, C312, R319, R320, Q308 and Q309. The second, also a two pole stage, is made up of C314, C315, R324, R325, Q310, and Q311.

The low pass portion includes three stages. The first is a single pole stage made up of R330 and C318 in conjunction with Q312 and Q313. The second is a two pole stage comprising R334, R335, C320, C348, Q314, and Q315. The last is an active filter using an operational amplifier (CA3047). This circuit has a twin "T" notch at 4.7 kHz. Its null is determined by C401, C402, C403, R401, R402, and R407.

In order to maintain a transfer ratio of one across the filter, an attenuating network comprised of R408 and R410 brings the output through C409 to pin 9. R411 provides C409 a discharge path to ground.

2200-3400 Hz Filter: This filter is made up of separate high and low pass filters. Each contains three two pole stages, giving a total of six poles.

Output Amplifier (6.2.12)

Integrated circuit operational amplifier A3 is used as a dc to 20 kHz 25 dB gain amplifier. Resistors R68 and R70, in parallel with either R109, R110, R112, or R113, are used as a voltage divider between the output of A3 and the input signal to drive the inverting input, thereby establishing gain. Resistor R72 is used to bias the non-inverting input to A3. Capacitors C23 and C24 are used for frequency compensation. Resistors R67 and R69 and capacitors C25 and C26 are used as decoupling networks from the power supplies to A3. Since the output impedance of A3 is virtually zero ohms, parallel resistors R64 and R65 establish the proper source impedance to transformer T2.

Dc Rectifier and Dc Amplifier (6.2.12)

In order to provide dc control voltage for AGC amplifier A6, the ac output of A3 at the transformer T2 primary section is sampled through R66, converted to dc, and amplified. Diodes CR1 and CR2 and capacitors C28 and C29 form a voltage doubler rectifier which provides a dc input to amplifier A4 proportional to the ac output from the transformer. Integrated circuit operational amplifier A4 is used as a dc amplifier with differential inputs. The inverting input is provided by the dc reference voltage at the arm of potentiometer R74. Resistors R71, R76, R77, and R81 are used as voltage dividers to the inverting and non-inverting inputs of A4 to provide the differential gain of 40 dB. Capacitors C32 and C31 are used for high frequency compensation. Capacitor C49 and resistor R79 are used to provide an extremely low frequency roll-off. Resistors R75 and R80 and capacitors C30 and C34 are used as decoupling networks to the power inputs to A4. Diode CR3 is used to compensate for the temperature coefficient of the diodes in the voltage doubler rectifier. Diode CR4 is used to prevent the input to A6 from becoming a positive voltage. Resistor R82 and capacitor C35 are used as a filter network to the input of A6. The operation of A4 is such that it provides a dc voltage to terminal 2 of A6 so that the gain of A6 is increased or decreased, maintaining the dc voltage at TP7 equal to the dc reference voltage at TP6. The dc reference voltage at TP6 being established from a highly stable source, the signal output of transformer T2 is held constant.

Balancing Transformers and Hybrid (6.2.12)

The resistive hybrid used in the test set is comprised of network com-

using capacitor C14 and resistor R32 or R33 and capacitor C16 with resistor R34 or R35, and with internal balancing networks made up of capacitor C15 and resistor R36 or R37. These internal networks are connected in the circuit when the front panel NETWORK switch is positioned at INT. Transformers T1 and T2 are used to balance the hybrid network. The impedance seen looking into terminals 3 and 4 of transformers T1 and T2 is 600 ohms; therefore, when the TEST LOCATION switch is put on the 900 ohms position, two 150 ohm resistors R62 and R63 are placed in series with terminals 3 and 4 of T2 raising the input impedance to 900 ohms, likewise , two 150 ohm resistors R5 and R6 are placed in series with terminals 3 and 4 of T1. This must be done to properly drive and terminate the hybrid. Capacitors C1, C2, C21, and C22 are used to block dc currents from the test set. Varistors CR18 and CR19 are used to protect the transmit and receive circuits from high voltage ac signals (ringing). Capacitors C61 and C62 are used to compensate for the impedance of C21 and C22.

Resistors R1-R2-R3-R4 form a 12 dB balanced pad which is used in the 4-wire mode to duplicate the trans hybrid loss in the 2-wire mode.

3.3 Receiver

.1 Meter Attenuator (ADD dB) and Amplifier (6.2.12)

Resistors R8 through R16 form a five-position attenuator with four 10 dB steps. The front panel indication is used in conjunction with the meter indication to determine return loss.

Integrated circuit operational amplifier A1 is used as a dc to 20 kHz 55 dB amplifier. Resistors R18, R19, R22, and R23 form a voltage divider between the output of A1 and the inverting input to establish gain. Resistor R17 provides the bias for the non-inverting input. Capacitors C4 and C5 are used for high frequency compensation. Resistors R20 and R21 and capacitors C6 and C7 are used as decoupling networks to the power supply inputs.

.2 THL Correction Amplifier and Pads (6.2.12)

Integrated circuit operational amplifier A2 is connected as a non-inverting 23-33.8 dB gain amplifier. Resistors R27, R28, R47 through R61, and R31 form a switchable voltage divider network to adjust the gain of the amplifier. Resistors R47 through R50 control the gain in 0.2 dB steps and resistors R52 through R61 control the gain in 1.0 dB steps. Resistor R26 is used to provide the input bias to the non-inverting input (as well as being part of the input attenuator). Capacitors C10 and C11 provide high frequency compensation. Resistors R29 and R30 and capacitors C12 and C13 are used as decoupling networks to the power supply inputs. Resistors R116 and R26 are used to provide 3.5 dB loss with switch S2 in the +23 dB position. Resistors R24 and R26 are used to provide 26.5 dB loss with switch S2 in the +0 dB position.

3.3.3 Meter Driver Amplifier (6.2.12)

Integrated circuit operational amplifier A7 is connected as an ac amplifier with a full wave bridge rectifier network and dc meter in its feedback network. The output of A7 (terminal 3) drives a full wave bridge rectifier composed of CR6, CR9, CR12, and CR13. The positive output of this bridge is established at the junction of CR6 and CR12. The current established due to the rectifier drives the dc meter up-scale left via R118 through R123. A reversed bias to the meter allows the expanded signal characteristic controlled by the resistor-diode network, which consists of resistors R100-R101-R102-R103-R105-R106-R107-R108 and diodes CR14-CR15-CR16-CR17. Diode CR15 is a 10 V Zener diode which establishes a stable reference potential while diodes CR14, CR16, and CR17 are used for temperature compensation of the reference voltage. Diodes CR7 and CR8 are used to prevent the meter from being overloaded. Capacitors C43 and C52 filters the random noise signal being measured, minimizing the fluctuations of the meter. The balance of the feedback network to amplifier A7 is composed of resistors R93 and R94. Adjustment of R94 controls the forward current through the meter and adjustment of R103 controls the reverse bias current through the meter. Diodes CR10 and CR11 prevent latch-up of the amplifier under overload conditions. Capacitors C44 and C45 are used for high frequency compensation. Resistors R98 and R99 and capacitors C46 and C47 are used as decoupling networks to the power supply inputs. Resistor R92 is used to provide the bias to the non-inverting input to A7.

3.4 Power Supplies

.1 Ac Input Power Supply (6.2.8)

This power supply is used to provide filtered and regulated +12 V and -12 V for internal test set operation from a main supply of 115 V ±10% 60 Hz ac. This circuit is composed of a power cord input, line fuse, line power switch, and center-tapped step-down transformer T201. T201 drives a full wave bridge rectifier assembly which provides positive 20 V dc to TP204 and negative 20 V dc at TP205. Capacitors C206 and C207 are filters for the full wave dc provided by the rectifier assembly CR201.

+12 Volt Regulator

The +12 volt regulator is composed of series pass transistor Q204, amplifier transistor Q205, and voltage reference diode CR205. The 12 V dc output voltage is established by summing up the reference voltage of CR205, the Vbe potential of Q205, and the forward bias potentials of CR203 and CR204. Resistors R210 and R211 provide base current for Q204 and collector current for Q205. Capacitor C207 further removes the ripple from the current through R210 and R211. Resistor R214 establishes the proper bias current for Zener diode CR205.

If the voltage at TP208 attempts to rise, since there is a constant voltage drop across CR205, the base voltage of Q205 will rise, increasing its base current. This increase in base current will increase its collector current. The total current through R211 is made up of the base current through Q204 and the collector current of Q205; therefore, an increase in the collector current of Q205 will decrease the base current of Q204 while the current through R211 remains constant. A decrease in base current of Q204 will decrease its emitter current, reducing the current through the load, which will tend to reduce the voltage at TP208 and achieve the regulating action.

Diodes CR203 and CR204 and the base emitter junction of Q205 serve to compensate the temperature coefficient of CR205.

-12 Volt Regulator

The -12 volt regulator consists of series pass transistor Q207 and amplifier transistor Q206. Resistors R212 and R213, with capacitor C210, provide filtered current for the base of Q207 and the collector of Q206. The voltage divider composed of R216 and R217 is designed to establish a negative 0.7 V dc potential at TP209 when there is positive 12 V dc at TP208 and negative 12 V dc at TP210.

The action of the -12 V regulator is similar to the +12 V regulator except that the voltage at TP209 is used as the reference. The action of this regulator is such that the negative voltage will track the absolute value of the positive voltage regulator with a negative potential. For example, if the positive voltage output were to become +12.5 V, then the negative output voltage would be -12.5 V. Effectively, the positive voltage regulator establishes the voltage control and the negative regulator merely tracks in the opposite polarity.

.2 -48 Volt Input Power Supply (6.2.11)

The purpose of this circuit is to provide ±12 V dc with respect to ground from a -48 V dc input supply having a positive ground. The ground of the ±12 V supply is common to the positive ground of the -48 V input supply.

Switch S1 is the front panel PWR switch.

Unijunction transistor Q200 and transistor Q201 form an astable multivibrator operating at approximately 200 Hz. Resistors R201 and R204 and capacitor C201 form a voltage divider to provide filtered -28 V (with respect to ground) at their common junction. The operation of the astable multi-vibrator is as follows: assuming that the emitter of unijunction Q200 is non-conducting and transistor Q201 is conducting, the potential at TP201 will be at -47.3 V dc. Capacitor C202 will charge through resistor R203. The voltage at TP200 increases until the unijunction fires and the voltage at TP200 abruptly returns to -47 V. At the instant the unijunction fires, the voltage at TP201 goes negative with respect to the emitter of Q201, turning off Q201. When Q201 turns off, its collector voltage

switches to ground potential. At this time, C202 charges through R201 and the emitter of Q200 until the potential at TP201 is positive with respect to the emitter of Q201. At this point, Q201 turns on and its collector voltage switches to -48 V. The time constants of this circuit are selected to provide a square wave with a 200 Hz repetition rate and a 50% duty cycle.

The collector voltage of Q201 is used to drive a pair of transistors used as a complementary switch. When the potential at TP202 is at -48 V, Q202 is non-conducting and Q203 is saturated. This action provides a 48 V peak to peak square wave, driven from a very low impedance source at TP 203 The square wave at TP203 is coupled through capacitor C205, diodes CR201, CR202, and filter capacitors C206, C209, to provide +24 V dc at TP204 and -24 V dc at TP205.

The operation of the ±12 V regulators is the same as that of the AC Input Power Supply.

Circuit Differences, L3 and L4 Sets

.1 Inputs

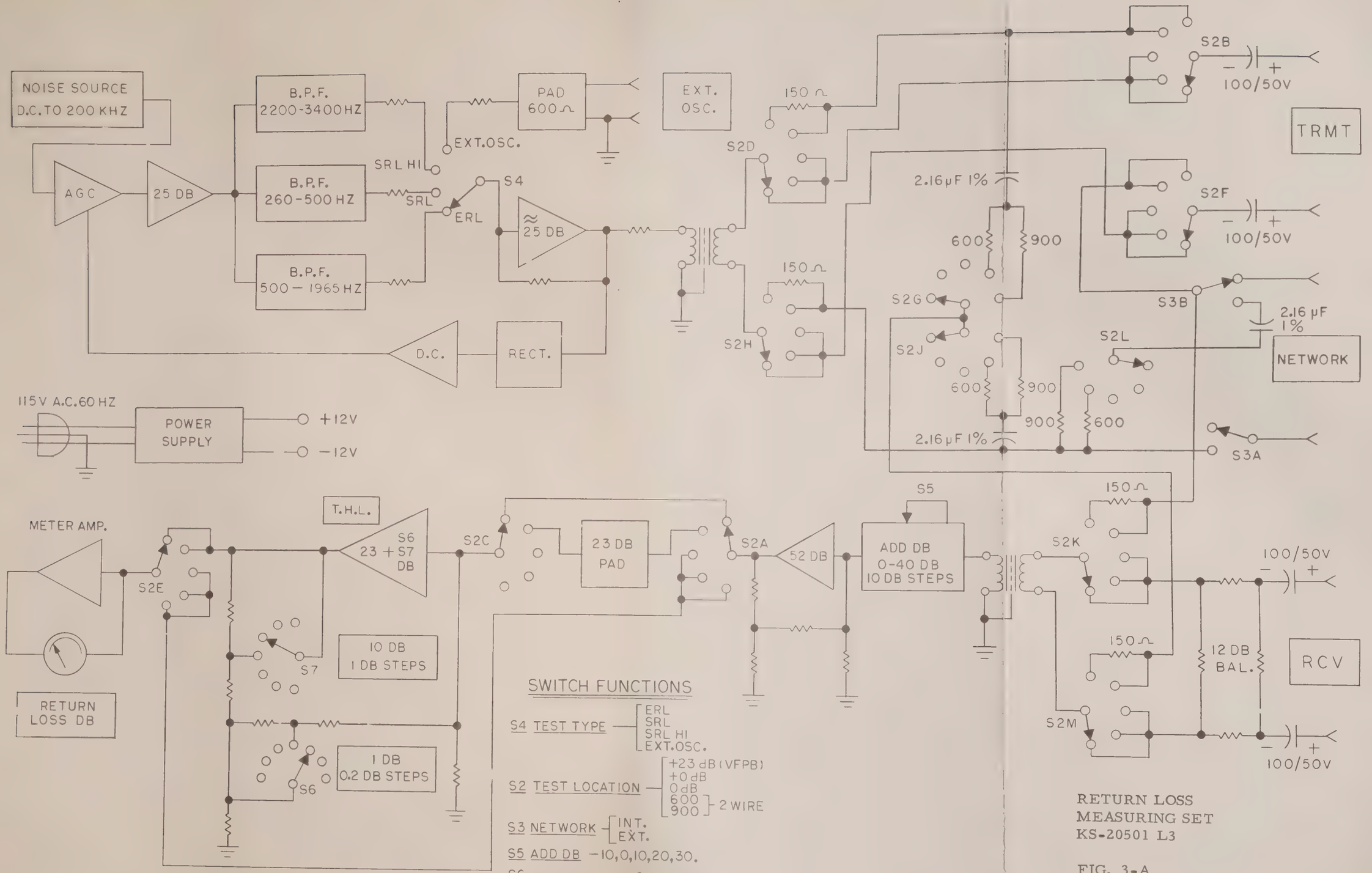
Any connection made to external lines or equipment on the L3 test set is made at the front panel by way of a 310-type telephone jack or General Radio-type binding post.

All external connections to the L4 test sets are made by way of a rear panel cable connector. (See Par. 2.3.2.)

.2 Power Supplies

The internal power supply for the L3 test set is powered from the external 115 V rms 60 Hz power mains through a power cord extending from the front panel.

The internal connections to the L4 test set power supply are powered from an external -48 V dc supply. The power input to the unit is made by the means of the rear cable connector. (See Par. 2.3.2.)



SWITCH FUNCTIONS

S4 TEST TYPE — ERL, SRL, SRL HI, EXT.OSC.

S2 TEST LOCATION — +23 dB (VFPB), +0 dB, 0 dB, 600 2 WIRE, 900 2 WIRE

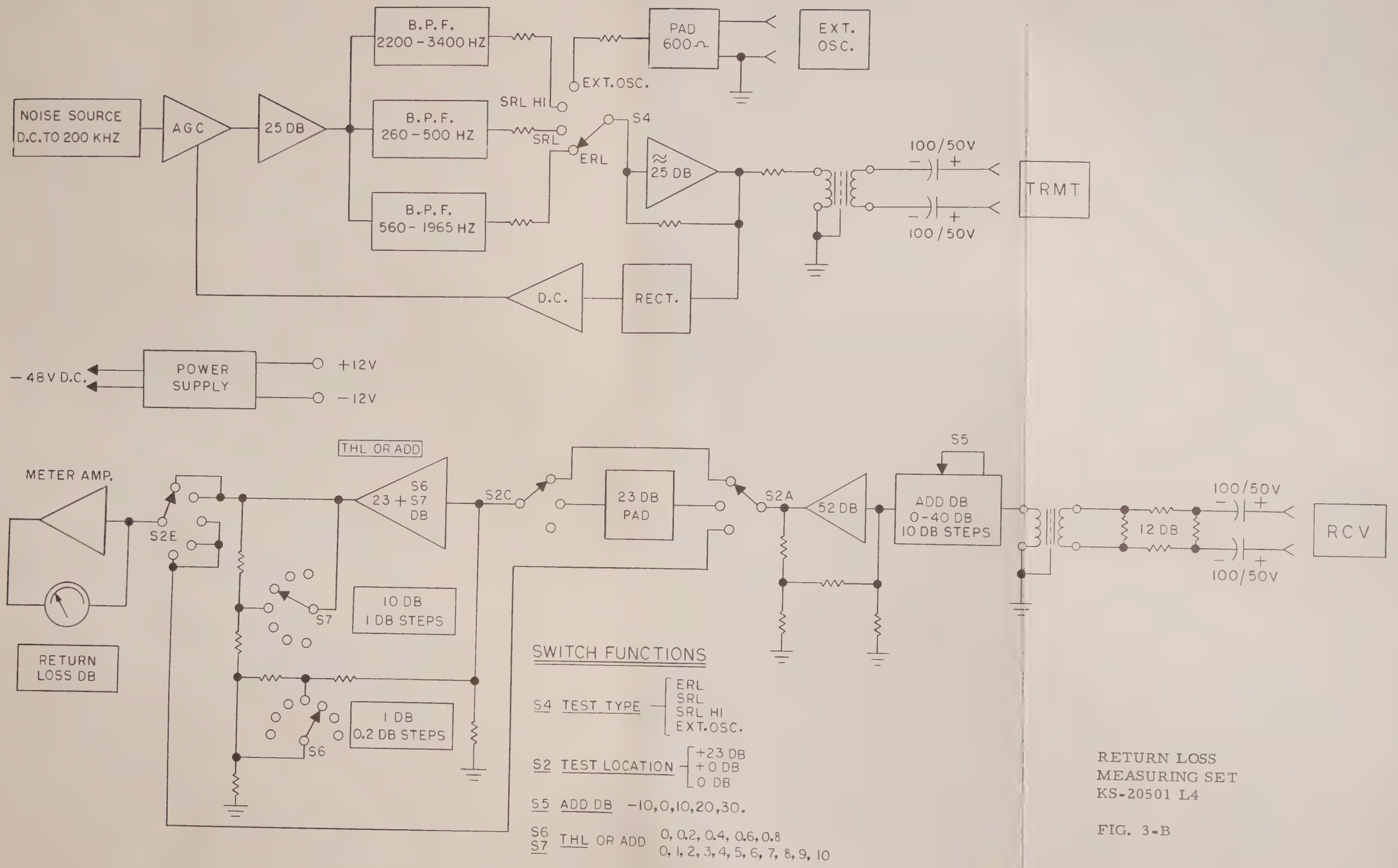
S3 NETWORK — INT., EXT.

S5 ADD DB — −10, 0, 10, 20, 30.

S6 S7 THL OR ADD — −0, 0.2, 0.4, 0.6, 0.8. 0, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10.

RETURN LOSS
MEASURING SET
KS-20501 L3

FIG. 3-A



RETURN LOSS
MEASURING SET
KS-20501 L4

FIG. 3-B

4.0 MAINTENANCE

4.1 Introduction

This section contains maintenance and service information for the [illegible] L3 and L4 Return Loss Measuring Sets: Performance Checks, and Calibration and Adjustment Procedures, are included.

4.2 Test Equipment Required

The test equipment required for maintenance of the Return Loss sets is outlined in Table I; listed are the types of equipment to be used, the critical specifications, and the recommended commercially available units.

4.3 Cabinet Removal

.1 To remove the L3 Test Set from its case:

.a Turn the PWR switch to OFF and disconnect the power cord from the power source.

.b With the unit in the normal operating position, remove the cover, unwind the power cable, loosen the four #10 oval slotted captive screws until the panel is free from the case.

.c Turn the instrument upside-down on a padded surface; then lift the case from the electronics portion (front panel).

.d Reverse the procedure to replace the case.

.2 To remove the L4 Test Set from its dust cover, remove the six No. 6 slotted captive screws.

4.4 Performance Checks

The performance checks are to be performed with the Return Loss Test Sets in the case (L3) or the dust cover (L4). These procedures are designed to be used for periodic maintenance, incoming quality control checks, and to check specifications after a repair.

CAUTION

When replacing the power cable in the cover of the portable set, take care that the three-prong plug is first placed under the left retaining tab before completely winding the cord so as to prevent a possible jamming of controls.

TEST EQUIPMENT REQUIRED

INSTRUMENT TYPE	REQUIRED CHARACTERISTICS	USE	RECOMMENDED MODEL
RMS Voltmeter	Frequency Range: 10 Hz to 10 MHz Accuracy: ± 1% 50 Hz to 1 MHz Voltage Input: 0.001 to 300 V	Output Level	Hewlett-Packard 3400A
Wave Analyzer	Frequency Range: 20 Hz to 50 kHz Band Width: 10 Hz Accuracy of Calibration: ± 1/2% +5Hz	Filter Characteristics	General Radio 1900-A
Audio Oscillator	Frequency Range: 5 Hz to 600 kHz Impedance: 600 Ω Max. Distortion: 0.2% 20 Hz to 200 kHz	External Oscillator Frequency Response Receiver Sensitivity Receiver Frequency Response Longitudinal Balance Filter Characteristic Check ERL, SRL, SRL HI Filter Adj. Output Impedance Adj. Input Impedance Adj. Meter Sensitivity Adj.	Hewlett-Packard 200CD
Vacuum Tube Voltmeter	Accuracy: within ± 1% of full scale Meter: linear expanded dB scale Calibration: 1 mW in 600 Ω	External Oscillator Frequency Response Receiver Sensitivity Receiver Frequency Response Longitudinal Balance Filter Characteristic Check ERL, SRL, SRL HI Filter Adj. Output Impedance Adj. Input Impedance Adj. Meter Sensitivity Adj.	Hewlett-Packard 400L

Attenuator Set	Range: 0-111 dB in steps of 0.1 dB Accuracy: within 0.1 ± 1% dB at 1 kHz Impedance: 600 Ω	Receiver Sensitivity Filter Characteristics ERL, SRL, SRL HI Filter Adj. Meter Sensitivity Adj.	General Radio 1450-TBR
Voltmeter	Range: 5000 V rms 5000 V dc Accuracy: ± 2% V dc full scale ± 3% V ac full scale	Power Supplies Check	Simpson 260
Digital Frequency Counter	Frequency Range: DC to 32 MHz Accuracy: ± 0.3%	Filter Characteristic Check ERL, SRL, SRL HI Filter Adj.	General Radio 1192
Oscilloscope	Band Width: DC to 13 MHz Rise Time: 27 ns	Waveforms	Tektronix 531A CA Dual Trace Plug-In
0.05 μF capacitor	Accuracy: measured to ± 1% absolute	Network	
2.16 μF capacitor	Accuracy: ±1%	Accuracy 2-Wire	
Balancing Transformer		Longitudinal Balance	UTC A20
900Ω resistor	Accuracy: ±1%	Terminating Load	RN65C9000F
600Ω resistor	Accuracy: ±1%	Terminating Load	RN65C6000F
150Ω resistor	Accuracy: ±1%	Network	RN65C1500F
150Ω resistor	Accuracy: ±5%	Balance	RC20GF151J
Adapter	GR double-plug	Network	General Radio Type 274-MB
Test Leads	GR to GR, 24" L. GR to alligator, 24" L.		
900 Ω resistor	Accuracy: ± 0.1%	Network	

TABLE I

4.4 Performance Checks (Continued)

.1 Output Level

.a A true rms ac voltmeter, such as a Hewlett-Packard 3400A, a 900 Ω ± 1% resistor, and a 600 Ω ± 1% resistor are needed for this test.

.b Set TEST LOCATION switch to 0 dB and TEST TYPE switch to ERL.

.c Connect the 600 Ω resistor and the ac voltmeter across the TRMT terminals of the Test Set.

.d The average reading of the voltmeter, set to maximum damping, should be -2 dBm ± 0.2 dB.

.e Set TEST TYPE switch to SRL; the as voltmeter should read -2 dBm ± 0.2 dB.

.f Set TEST TYPE switch to SRL HI; the ac voltmeter should read -2 dBm ± 0.2 dB.

.g Set TEST LOCATION switch to 600 Ω and TEST TYPE switch to ERL, and replace the 600 Ω resistor across the TRMT terminals with the 900 Ω resistor; the ac voltmeter shall read -8 dBm ± 0.2 dB (assuming the voltmeter scale is calibrated for 600 Ω and 1 mW).

.2 Filter Characteristics

.a A wave analyzer, such as a General Radio 1900-A, with a 10 Hz measurement band width, and a 600 Ω ± 1% resistor are needed to perform this test.

.b Set TEST LOCATION switch to 0 dB and TEST TYPE switch to ERL.

.c Connect the wave analyzer input terminals and the 600 Ω resistor to the Test Set TRMT terminals.

.d Using the ERL filter characteristic as a guide, sweep the frequency band from 80 Hz to 5 kHz with the wave analyzer. Compare the resulting relative frequency characteristic with the ERL filter curve, FIG. 1-F. The two should be approximately the same. This is intended as a guide test since the analyzer is difficult to read when monitoring a gaussian noise signal. A more accurate check can be made by following the procedure given in the Calibration section.

.e Set TEST TYPE switch to SRL; repeat the spectrum measurement. Compare the result with the SRL HI filter characteristic in FIG. 1-H.

.3 EXT OSC Frequency Response

.a An audio oscillator, such as a Hewlett-Packard 200 CD, a VTVM such as a Hewlett-Packard 400 L, and a 600 Ω ± 1% resistor are needed for this measurement.

Set TEST LOCATION switch to 4-XB and TEST TYPE switch to EXT OSC.

Connect the audio oscillator to the EXT OSC terminals and the 600 Ω resistor and a VTVM across the TRMT terminals.

Set the oscillator output level to obtain a reading of 0 dB on the VTVM. Vary the oscillator frequency from 100 Hz to 15 kHz while checking to see that its output level is constant.

The maximum amplitude excursion at the TRMT terminals should not exceed .4 dB from 200 Hz to 5 kHz and 1 dB from 100 Hz to 15 kHz.

Receiver Sensitivity

A VTVM, such as a Hewlett-Packard 400 L, an audio oscillator, such as a Hewlett-Packard 200 CD, and an attenuator, such as a General Radio 1450-TBR, will be needed for this test. Connect the test equipment to the Test Set RCV terminals as shown in FIG. 4-A.

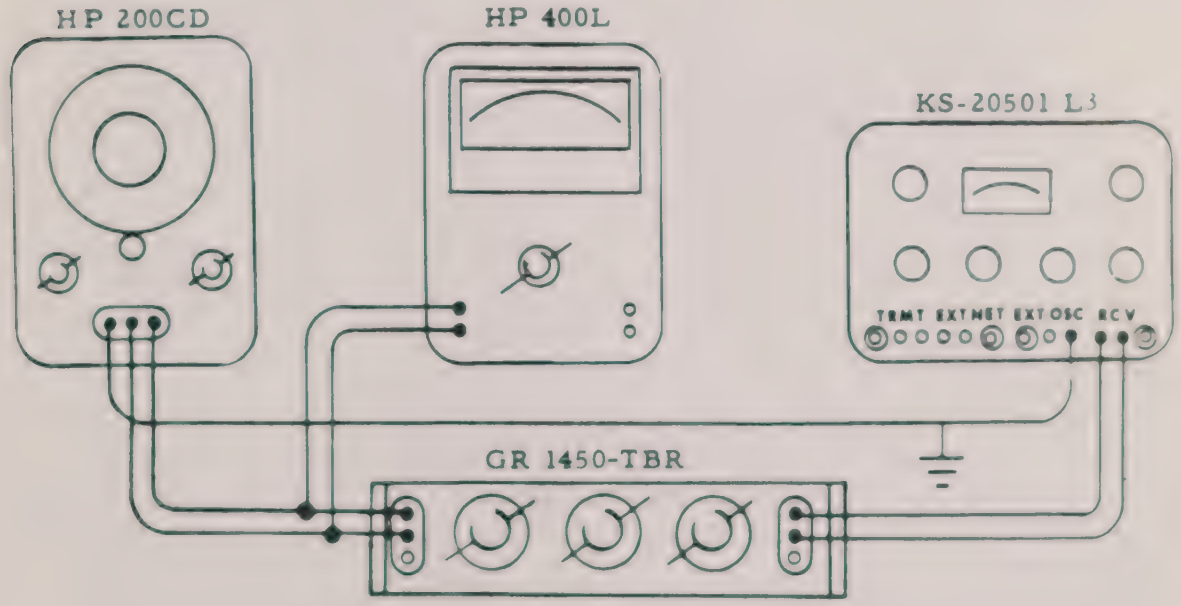


FIG. 4-A

NOTE: Test Set should be grounded to signal source through EXT OSC ground terminals.

Set TEST LOCATION switch to +0 dB, THL switch to 10.0 dB, and ADD dB switch to -10.

With the attenuator set to 0 dB, adjust the audio oscillator output level (at 1 kHz) to obtain a Test Set RETURN LOSS dB meter indication of 0 dB. (Approximately -3 dBm output from the oscillator.)

4. 4. 4. d Set the Test Set and test equipment controls as shown in the following table. In each case the RETURN LOSS dB meter reading should be 0 ± 0. 1 dB.

TEST LOCATION	ADD dB	THL OR ADD 1 dB	THL OR ADD 0. 2 dB	ATTENUATOR
+0 dB	-10	10	0	0. 0
+0 dB	0	10	0	10. 0
+0 dB	10	10	0	20. 0
+0 dB	20	10	0	30. 0
+0 dB	30	10	0	40. 0
+0 dB	30	9	0	39. 0
+0 dB	30	8	0	38. 0
+0 dB	30	7	0	37. 0
+0 dB	30	6	0	36. 0
+0 dB	30	5	0	35. 0
+0 dB	30	4	0	34. 0
+0 dB	30	3	0	33. 0
+0 dB	30	2	0	32. 0
+0 dB	30	1	0	31. 0
+0 dB	30	0	0. 2	30. 2
+0 dB	30	0	0. 4	30. 4
+0 dB	30	0	0. 6	30. 6
+0 dB	30	0	0. 8	30. 8
0 dB	30	0	0	30. 0
+23 dB	30	0	0	53. 0

. e Set TEST LOCATION switch to 0 dB and ADD dB switch to 0. Set the attenuator 10. 0 ± 0. 1 dB with the audio oscillator referenced 1 kHz and level adjusted to obtain a 0 dB reading on the RETURN LOSS dB meter. Adjust the attenuator to obtain the required meter indication in the table below.

ATTENUATOR	RETURN LOSS dB Meter	ATTENUATOR	RETURN LOSS dB Meter
10. 5	0. 5	15. 5	5. 5
11. 0	1. 0	16. 0	6. 0
11. 5	1. 5	16. 5	6. 5
12. 0	2. 0	17. 0	7. 0
12. 5	2. 5	17. 5	7. 5
13. 0	3. 0	18. 0	8. 0
13. 5	3. 5	18. 5	8. 5
14. 0	4. 0	19. 0	9. 0
14. 5	4. 5	19. 5	9. 5
15. 0	5. 0	20. 0	10. 0

4.4.5 Receiver Frequency Response

.a An audio oscillator, such as a Hewlett-Packard 200 CD, and a VTVM such as a Hewlett-Packard 400 L, will be needed for this test.

.b Connect the oscillator and VTVM to the RCV terminals of the Test Set.

.c Set TEST LOCATION switch to 0 dB and ADD dB switch to 0.

.d Adjust the oscillator output level to provide an indication on the RETURN LOSS dB meter of 0 dB. (Approximately -3 dBm output from the oscillator at 1 kHz.)

.e Sweep the oscillator frequency from 100 Hz to 15 kHz and adjust the oscillator output level to keep the RETURN LOSS dB meter indication at 0 dB. Note the excursions of the oscillator output on the VTVM.

.f The maximum excursion (from maximum to minimum) of the oscillator output level shall be 0.4 dB from 200 Hz to 5 kHz; 1 dB from 100 Hz to 15 kHz.

.7 Longitudinal Balance

.a A VTVM, such as a Hewlett-Packard 400 L, an audio oscillator, such as a Hewlett-Packard 200 CD, a balancing transformer, such as a U.T.C. Model A20, and a 150 Ω ±5% resistor are needed for this test.

.b Connect the Test Equipment as shown in FIG. 4-B.

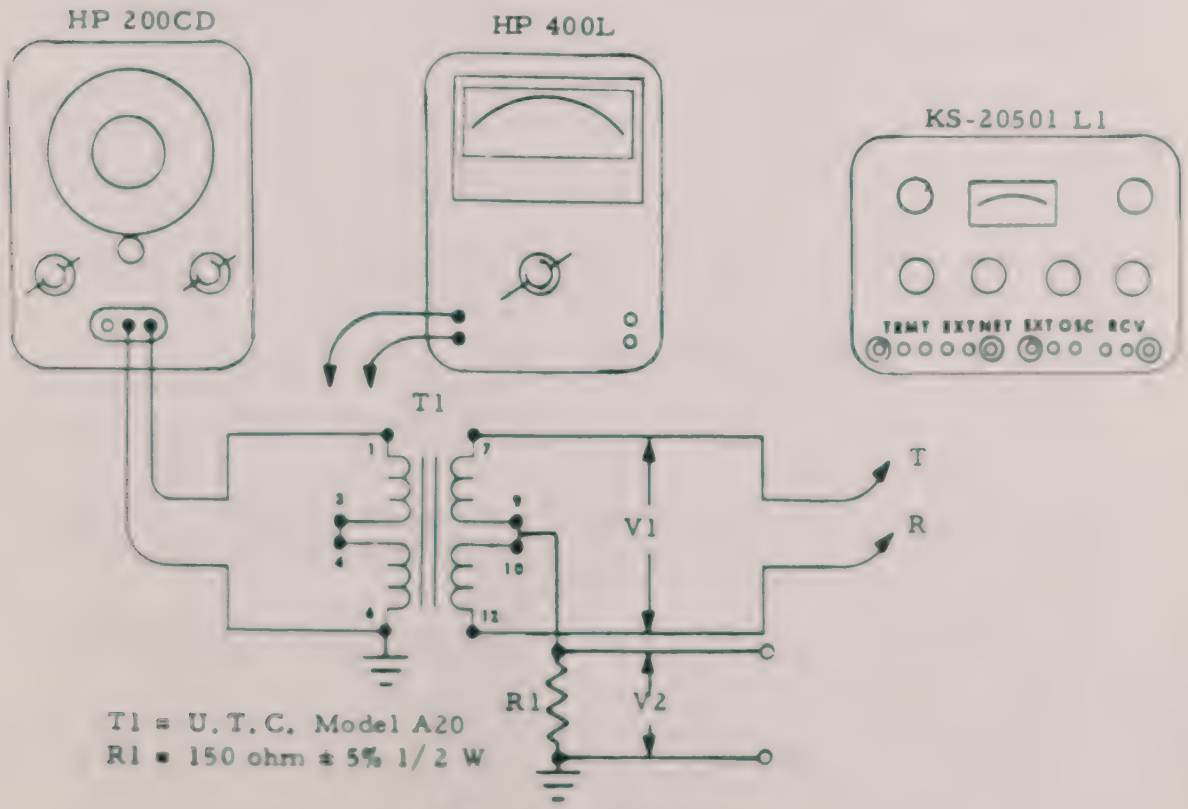


FIG. 4-B

4.4.6.c The longitudinal balance measurements are made by connecting the test circuit T and R terminals to the proper terminals of the Test Set; connect the VTVM across T and R to measure V_1 (150Ω resistor should not be grounded when measuring V_1; adjust the oscillator output level to obtain 0 dBm at V_1; remove the VTVM from V_1 and connect it to measure V_2. The absolute value of the voltage measured at V_2 in dB is the longitudinal balance at the frequency used; e. g. , V_2 = -65 dB, therefore balance = 65 dB.

.d Connect the T and R terminals of the test circuit to the TRMT terminals of the Test Set.

.e Set TEST LOCATION switch to 0 dB, TEST TYPE switch to EXT OSC, NETWORK switch to INT, and ADD dB switch to 0. Perform the longitudinal balance measurements at 100 Hz and 3000 Hz. The balance shall be greater than 70 dB at 100 Hz and 55 dB at 3000 Hz. Repeat these measurements with the TEST LOCATION switch in the 600 Ω and 900 Ω positions.

.f Set the TEST LOCATION switch to the 0 dB position and connect the T and R terminals of the test circuit to the RCV terminals of the Test Set. Repeat the measurements of the preceding paragraph.

.7 Hybrid Check (L3 only)

.a Set TEST LOCATION switch to 600 Ω, TEST TYPE switch to ERL, NETWORK switch to INT, and ADD dB switch to 0. The RETURN LOSS dB meter should indicate 0 ± 0. 2 dB.

.b Connect a shorting strap across the TRMT terminals or use a shorting type plug in the 310 jack. The RETURN LOSS dB meter should indicate 0 ± 0.2 dB.

.c Set TEST LOCATION switch to 900 Ω. The RETURN LOSS dB meter should indicate 0 ± 0. 2 dB.

.d Remove the short from the TRMT terminals or the 310 jack. The RETURN LOSS dB meter should indicate 0 ± 0.2 dB.

.8 Accuracy of 2-W Measurements (L3 only)

.a A 900 Ω ± 0. 1% resistor and a network composed of a 900 Ω ± 0. 1% resistor in parallel with a 0. 05 μF ± 1% capacitor will be needed for this test.

.b Set NETWORK switch to INT.

.c The test network is connected to the TRMT terminals and the Test Set is operated as shown in the following table. All Return Loss readings should be ± 0. 4 dB of those shown on the table.

TEST LOCATION	TEST TYPE	Test Network	Return Loss-dB
900	ERL	900 Ω	28.3
900	ERL	900 Ω//. 05 μF	15.7
900	SRL	900 Ω	18. 9
900	SRL	900 Ω//. 05 μF	23. 1
900	SRL HI	900 Ω	36. 6
900	SRL HI	900 Ω//. 05 μF	8. 9

4.4.9 Accuracy of 2-W Measurements (L? only)

.a Four 900 Ω ± 0.1% resistors, four 150 Ω ± 1% resistors, three 2.16 μF ± 1% capacitors, and one 0.05 μF ± 1% capacitor will be needed for this test.

.b A Test Hybrid is composed of three 900 Ω resistors and three 2.16 μF capacitors, as shown in FIG. 4-C.

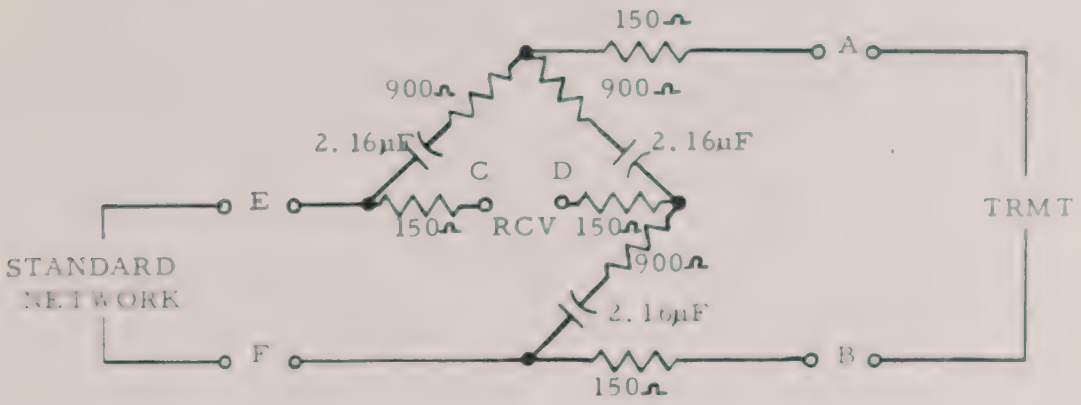


FIG. 4-C

.c Connect the Transmit terminals to A and B; the Receive terminals to C and D.

.d Set TEST LOCATION switch to +0 dB, THI switch to 10.0 dB, and TEST TYPE switch to ERL.

.e Without the Test Standard Network connected to the Test Hybrid, the Test Set should read approximately 8 dB. Note the actual reading of the Test Set as this will be used as a reference.

.f Connect the Standard Network (composed of either a 900 Ω resistor or a 900 Ω resistor in parallel with a 0.05 μF capacitor) to terminals E and F of the Test Hybrid and note the Test Set reading. The difference between this reading and the reference reading taken in the preceding step is the return loss.

.g Repeat the test for the conditions shown in the following table. The return loss indicated on the Test Set should be within ± 0.4 dB.

TEST LOCATION	TEST TYPE	THI OR ADD	Return Loss-dB
+0 dB	ERL	10.0	28.3
+0 dB	ERL	10.0	15.7
+0 dB	SRL	10.0	18.9
+0 dB	SRL	10.0	23.1
+0 dB	SRL HI	10.0	36.6
+0 dB	SRL HI	10.0	8.9

4.5 Calibration and Adjustment Procedures

Remove the Return Loss Test Set from the carrying case (L3) or from the dust cover (L4) as instructed in Section 4.3 The calibrations are performed with the instruments powered in the following manner: the L3 portable model from a power source of 115 V, 60 Hz; the L4 rack mount model from a -48 V dc source with connection made through the rear cable connector.

.1 Power Supply

A check of the +12 V and -12 V supplies for nominal value will suffice. A voltmeter, such as the Simpson 260, and a pair of alligator clip leads about 24 inches long will be required for this testing.

.2 +12 Volt Supply Check

Connect the dc voltmeter to test point TP208 and the common lead to the chassis. The voltmeter should read +12.0 ±.70 V.

.3 -12 Volt Supply Check

Connect the dc voltmeter to test point TP210 and the common lead to the chassis. The voltmeter should read -12.0 ±.70 V.

.4 Filter Characteristics Check

An audio oscillator, such as a Hewlett-Packard 200CD, an attenuator, such as a General Radio 1450-TBR, a VTVM, such as a Hewlett-Packard 400L, and a digital frequency counter, such as a General Radio 1192, will be required to measure the filter characteristics. See FIG. 4-D.

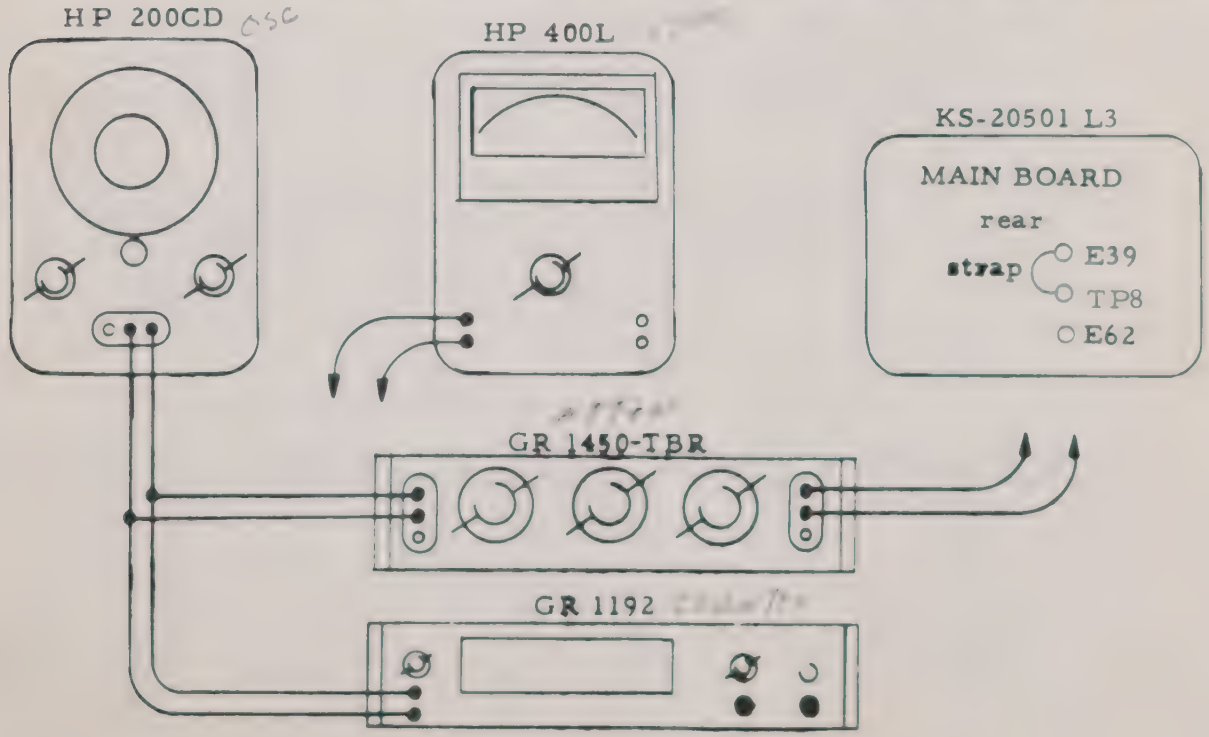


FIG. 4-D

4.5.4.a The filters are adjusted at the factory to have the frequency characteristics shown below. If the deviations observed are outside the tolerances given, the set should be returned to the manufacturer for repair.

.b Remove the strap connecting tie points E39 and E38 (TP8) on the main assembly board.

.c Adjust the oscillator output to a level of approximately -3 dBm at 350 Hz; then set the attenuator for a 30 dB loss.

.d Connect the attenuator output to tie point E39, the common to ground tie point E62 (reference 6.2.12).

.5 SRL Filter

.a Connect the VTVM between the collector of Q307 and ground tie point E62 or chassis.

.b Adjust the oscillator output level at 360 Hz to obtain an indication of -10 dBm on the VTVM.

.c Sweep the oscillator output frequency from 100 Hz to 1,000 Hz. The output level as monitored on the voltmeter should follow the SRL characteristic given below; if a deviation from specification is apparent, see par. (4.5.4.a)

Frequency-Hz	Loss-dB *	Tolerance-dB
≦120	>20	-
200	9.5	±1.1
260	3	±0.5
360	0	±0.2
500	3	±0.5
650	10	±1.2
≧1000	>20	±1.2

* Excluding any insertion loss measurements.

.6 ERL Filter

.a Connect the VTVM to the terminal of E71 using tie point E62 or 1546414 for ground.

.b Adjust the oscillator output level at 1 kHz to obtain an indication of -10 dBm on the VTVM.

.c Sweep the oscillator output frequency from 50 Hz to 5 kHz. The input level, as monitored by the VTVM, should follow the ERL characteristic given below; if a deviation from the specification is apparent, see par. (4.5.4.a)

Frequency-Hz	Loss-dB *	Tolerance-dB
≦200	>30	-
300	21.8	±2.3
560	3	±0.4
750	0	±0.1
1000	0	±0.1
1500	0	±0.1
1965	3	±0.4
2400	10.9	±1.2
3000	~~32.0~~ 22.9	±3.0
4000	42.6	±5.0
≧5000	>45	-

4.5.7 SRL HI Filter

.a Connect the VTVM to the collector of Q327, using tie point E62 or chassis for ground.

.b Adjust the oscillator output level at 2.7 kHz to obtain an indication of -10.0 dBm on the VTVM.

.c Sweep the oscillator output level from 1.5 kHz to 5 kHz. The output level as monitored by the VTVM should follow the SRL HI filter characteristic shown below; if there is a deviation from this specification, see par. (4.5.4.a)

Frequency-Hz	Loss-dB *	Tolerance-dB
≦1300	>30	-
2000	11.5	±1.3
2200	3	±0.5
2700	0	±0.2
3400	3	±0.5
3700	10.9	±1.3
≧5700	>30	-

.d Replace the strap connecting tie points E39 and E38 on the main assembly board.

.8 Output Impedance

An audio oscillator, such as a Hewlett-Packard 200CD; a VTVM such as a Hewlett-Packard 400L; and a 600 Ω ±1% load resistor will be required to measure the output impedance. See FIG. 4-E.

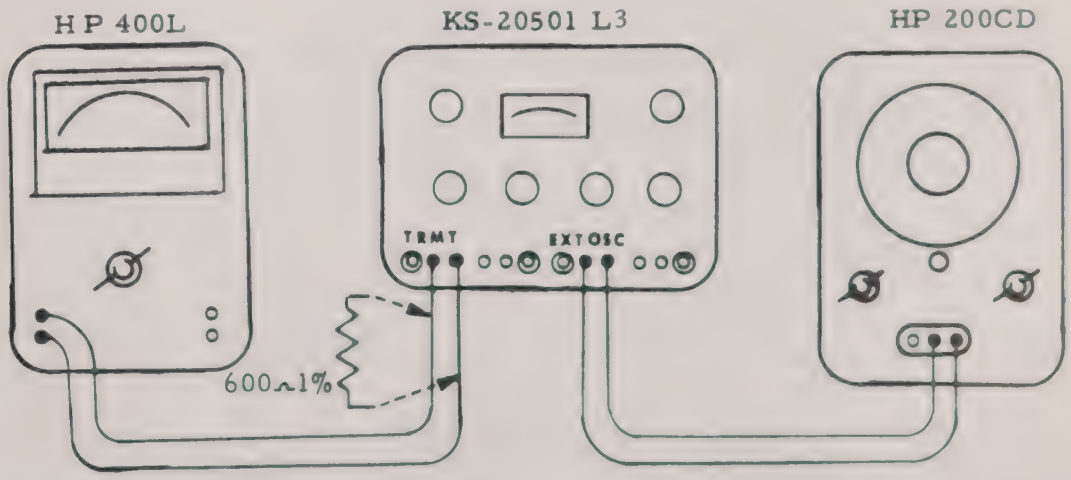


FIG. 4-E

.a Set the TEST LOCATION switch to 0 dB and the TEST TYPE switch to EXT OSC.

* Excluding any insertion loss measurements.

* L4 is E37 & E62

.4.8.b With the audio oscillator output connected to the EXT OSC terminals and the VTVM monitoring the output of the TRMT terminals, adjust the oscillator level to obtain a VTVM indication of 0 dBm at 1 kHz. (this is an oscillator output of approximately -6 dBm.)

.c With a 600 Ω ± 1% load resistor across the TRMT terminals, a level of -6 dBm±0.1 dB should be observed on the VTVM. The components determining the output impedance are factory selected; if the requirement is not met, the set should be returned to the manufacturer for repair.

.9 Input Impedance

An audio oscillator, such as a Hewlett-Packard 200 CD; a VTVM such as a Hewlett-Packard 400 L; and a 600Ω±1% load resistor will be required to measure the input impedance. See FIG. 4-F.

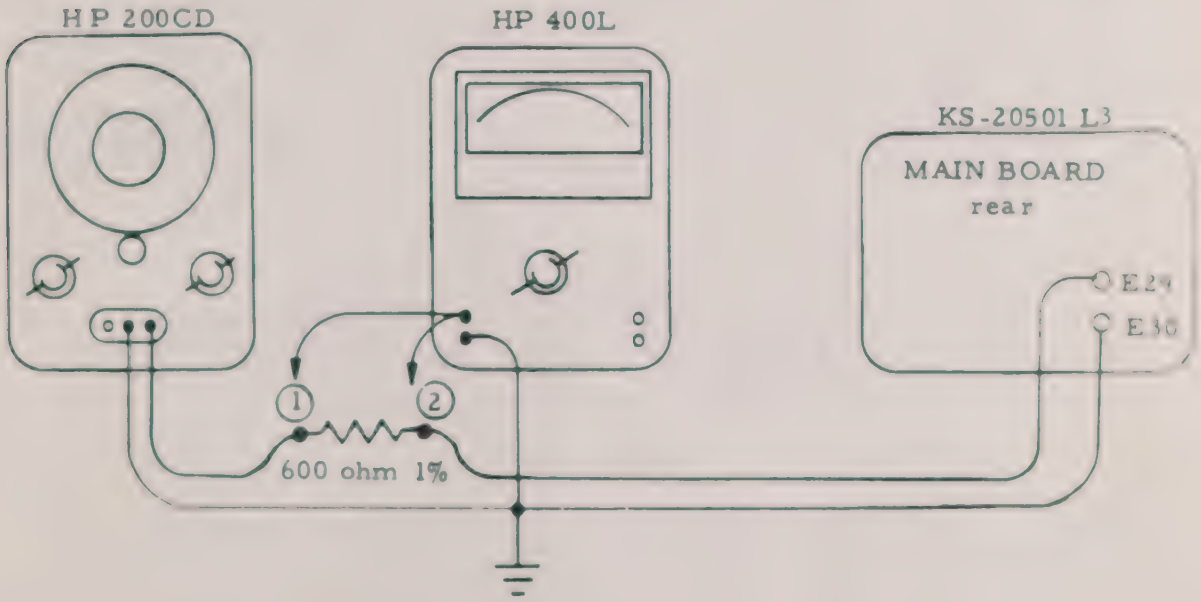


FIG. 4-F

.a Remove the shorting strap from between tie points E29 and E83 on the main board.

.b Connect the test equipment to the Test Set as shown in FIG. 4-F.
NOTE: Use caution to assure that the ground return is properly established.

.c With the 600 Ω ± 1% load resistor connected in series, and the VTVM connected across the audio oscillator Position 1, adjust the oscillator to obtain a level of 0 dBm at 1 kHz. Move the VTVM connection to Position 2 and monitor the input to the Test Set and check for a loss of -6 dB ± 0.1 dB. The components which determine the input impedance are factory selected. If the requirement is not met, the set should be returned to the manufacturer for repair.

4.5.10 Meter Sensitivity

An audio oscillator, such as a Hewlett-Packard 200 CD; an attenuator, such as a General Radio 1450-TBR; and a VTVM, such as a Hewlett-Packard 400 L; will be required to measure the meter sensitivity.

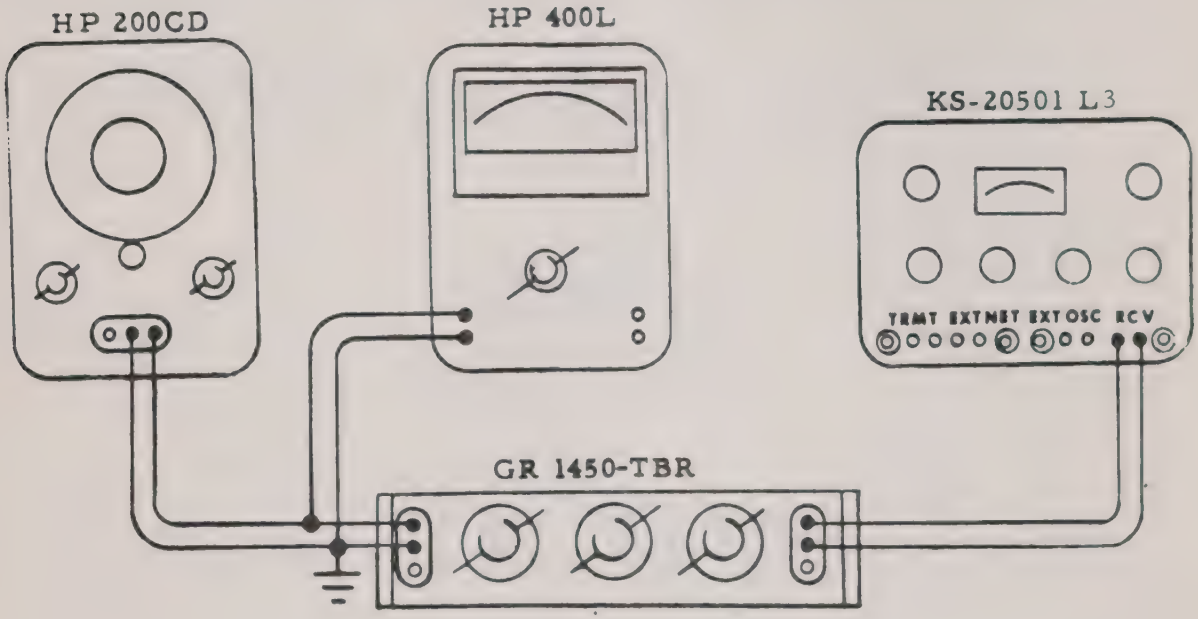


FIG. 4-G

.a With the TEST LOCATION control in the 0 dB position and the ADD dB rotary switch set to 0, connect the test equipment as shown in FIG. 4-G.

.b Set the attenuator to 00.0 and adjust the oscillator level at 1 kHz to obtain a -3 dBm reading on the VTVM.

.c Adjust the R94 METER 0 dB ADJ to obtain a 0 dB indication on the RETURN LOSS dB meter.

.d Switch the attenuator to 10.0 dB and adjust the R103 METER 10 dB ADJ potentiometer to obtain a 10.0 dB indication on the RETURN LOSS dB meter. Repeat the measurements and adjust R94 and R103 until the 0 dB and 10 dB positions are accurately reflected by the pointer.

.11 Output Level, L3

Set the controls on the Return Loss Measuring Set to the following positions: TEST LOCATION to 600; TEST TYPE to ERL; NETWORK to INT; ADD dB to 0. Adjust potentiometer R74 to obtain a 0.0 dB indication on the RETURN LOSS dB meter.

5.12 **Output Level, L4**

Set the controls on the Return Loss Measuring Set to the following positions: Test Location to 0 dB TEST TYPE to ERL; and ADD dB to 0. Complete the loop connection between TRMT and RCV using the appropriate cable. Adjust potentiometer R74 to obtain a 0.0 dB indication on the RETURN LOSS dB meter.

5.0 TROUBLESHOOTING TECHNIQUES

5.1 General

This section is designed to aid in the isolation of possible malfunctions of the equipment. The outlined procedures should be used after it has been established that the instrument is not operating to the standards delineated in Performance Checks, Section 4.4, or cannot be calibrated to the standards in Calibration Procedures, Section 4.5. Familiarity with the overall operation of the instrument, Section 3.0, and the detailed operation of the individual units, Section 2.2, is a prerequisite. Any malfunction should be related to the most probable area and traced back to its source; typical voltages and waveforms, shown in Section 6.0, represent key points in the instrument and should be used as aids to localization. Troubleshooting from Front Panel Symptoms, Section 5.2, contains a summary of RETURN LOSS dB meter indications which may be classified as pointing to instrument malfunction, as well as procedures that may be helpful in isolation of the probable cause. Isolating Malfunctions, Section 5.3, contains a progressive diagnostic table based on specific section malfunctions as they relate to the typical voltages and waveforms shown with the schematics.

The voltages and waveforms shown with the schematics are based on the following control positions and/or signal inputs, with ac and dc measurements taken between test point and ground terminal E202.

PWR	ON
THL OR ADD	0.0
TEST LOCATION	+0 dB
TEST TYPE	ERL
ADD dB	0
NETWORK	INT

For the Receive Section of the instrument, apply a 1 kHz single tone signal to the RCV terminals at -8 dB level for measuring voltages or observing waveforms at test points TP1, TP2, and TP3.

For the Transmit Section of the instrument, remove the 1 kHz signal from the RCV terminals and connect a 600 Ω ± 1% resistor across the TRMT terminals for measuring voltages or observing waveforms at all remaining test points. Exceptions to be noted are the waveforms taken at TP4 with the TEST TYPE switch in the SRL and SRL HI positions respectively.

When servicing, remember that semiconductors are more prone to failure than any other components. Check the operation of transistors by establishing that they pass a signal and that the base emitter voltages are within about a volt of each other at all times when powered. Check that the resistance of diodes is high in one direction and low in the other; check that capacitors are

not shorted, and that they will pass an ac signal. Replace any component suspected of being defective to verify localization of a specific fault. A visual check for possible burned or loose components, loose connections, or any other obvious condition that would cause malfunction, should be performed.

The use of a pencil-type soldering iron with less than a 40 watt maximum capacity is recommended to prevent possible damage to the printed circuit board or components. If the iron is ac powered, use an isolating transformer between the iron and the source. Do not use a soldering gun as damaging voltages can be induced in components.

5.2 Troubleshooting from Front Panel Symptoms

.1 PWR to ON NETWORK to INT	ADD dB to 0 TEST LOCATION to 600
Meter does not read 0 dB on:	
a. TEST TYPE position ERL	Check ERL filter per Par. 4.5.6
b. TEST TYPE position SRL	Check SRL filter per Par. 4.5.5
c. TEST TYPE position SRL HI	Check SRL HI filter per Par. 4.5.7
d. None of the above	(1) Check the power source. (2) Check fuse F1. (3) Check Transmit Section per Section 5.1. (4) Check Receive Section per Section 5.1.

.2 PWR to ON NETWORK to INT ADD dB to 0	THL to 0.0 TEST LOCATION to +0 dB TEST TYPE to ERL
Meter does not read 0 or 10 when switching the ADD dB control from 0 to -10	Check meter sensitivity calibration per Par. 4.5.10

.3 PWR to ON ADD dB to -10 THL to 0.0	TEST LOCATION to +0 dB TEST TYPE to ERL RCV strapped to TRMT
a. Meter does not read 10 dB	(1) Check S5 (2) Check R8 through R16 (3) Check A1 and A2
b. Meter does not track proportionately when adjusting THL from 0 through 10	(1) Check S6 (2) Check R47 through R51
c. Meter does not tract proportionately when adjusting THL from .0 through .8	(1) Check S7 (2) Check R52 through R61

5. 4 Isolating Malfunctions

. 1 Power Supplies

+12 V supply does not read +12 ±0.70 V when checked per Par. 4. 5. 2.

L1: Using the information supplied on Schematic 6. 2. 8, check voltages and waveforms to isolate the malfunction.

L2: Using the information supplied on Schematic 6. 2. 11, check voltages and waveforms to isolate the malfunction.

-12 V supply does not read -12 ±0.70 V when checked per Par. 4. 5. 3.

L1: Using the information supplied on Schematic 6. 2. 8, check voltages and waveforms to isolate the malfunction.

L2: Using the information supplied on Schematic 6. 2. 11, check voltages and waveforms to isolate the malfunction.

. 2 Transmit Section

Transmit Section does not function.

L1: Use the information supplied on Schematic 6. 2. 12.

L2: Use the information supplied on Schematic 6. 2. 13.

L1 and L2: Check the voltages and waveforms using the following sequence of test points, to isolate malfunction to a specific area: TP9, 8, 13, 4, 5, 6, 7.

NOTE: If it becomes desirable to disable the feedback, remove the jumper connected the anode of CR4 and pin 2 of A6; next connect a -3.5 V dc voltage to pin 2 of A6, from a source impedance of less than 500 Ω to allow a fixed gain operation.

. 3 Receive Section

Receive Section does not function.

L1: Use the information supplied on Schematic 6. 2. 12.

L2: Use the information supplied on Schematic 6. 2. 13.

L1 and L2: Check the voltage and waveforms using the standard single tone signal, reference Par. 5. 1, and in the following sequence to aid in isolating a malfunction to a particular section: TP1, 2, 3, 10, 12.

NOTE: Reference Par. 4. 4. 4. d. Using the test set-up outlined in this paragraph, the following should be noted:

a. Steps 1-5 check the ADD dB switch.
b. Steps 6-14 check the THL 1 dB attenuator steps.
c. Steps 15-18 check the THL . 2 dB attenuator steps.
d. Step 19 checks the 0 dB wiring, the S2 pad, and amplifier A2.
e. Step 20 checks the +23 dBwiring switch S2 and the pad pad on S2.

6.0 DRAWINGS

6.1 General

This section contains the schematic diagrams with typical voltages and waveforms, supplemented by component and path locating diagrams, necessary to assist the field engineer or technician in the maintenance, calibration, and use of this equipment.

Notes

Unless otherwise specified: resistors are in ohms, 1/2 watt, 5%.
capacitors are in microfarads.

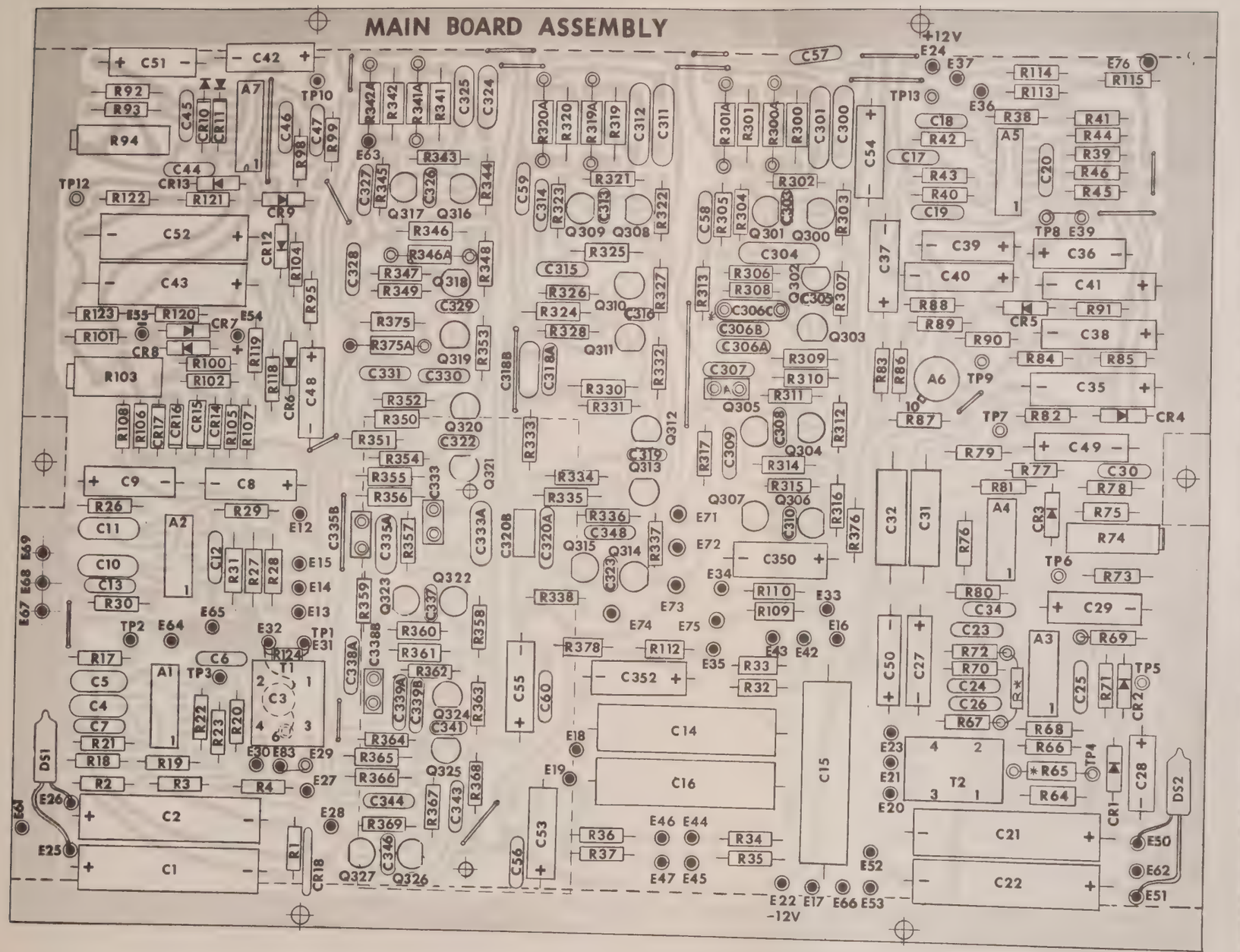
Components within broken lines (- - -) are mounted on printed circuit boards.

Nomenclature in blocks [ ] indicate front panel markings.

An asterisk * indicates that these values may be trimmed during test.

6.2 List of Drawings

6.2.1	Main Board, Component Side, L3
6.2.2	Main Board, Circuit Side, L3
6.2.3	Main Board, Component Side, L4
6.2.4	Main Board, Circuit Side, L4
6.2.5	Main Schematic, Filter Section, L3 and L4
6.2.6	AC Power Supply, Component Side, L3
6.2.7	AC Power Supply, Circuit Side, L3
6.2.8	AC Power Supply Schematic, L3
6.2.9	DC Power Supply, Component Side, L4
6.2.10	DC Power Supply, Circuit Side, L4
6.2.11	DC Power Supply Schematic, L4
6.2.12	Main Schematic, L3
6.2.13	Main Schematic, L4
6.2.14	Switch Detail Test Location L3 and L4
6.2.15	Switch Detail Add dB L3 and L4
6.2.16	Switch Detail THL OR ADD Attenuator L3 and L4
6.2.17	ERL Filter Board - Component Side
6.2.18	ERL Filter Board - Circuit Side



SEMICONDUCTOR BASING

Bottom View

Typical 2N3904, 2N3906

Bottom View

Typical 2N5138

Bottom View

Typical 2N5135

Bottom View

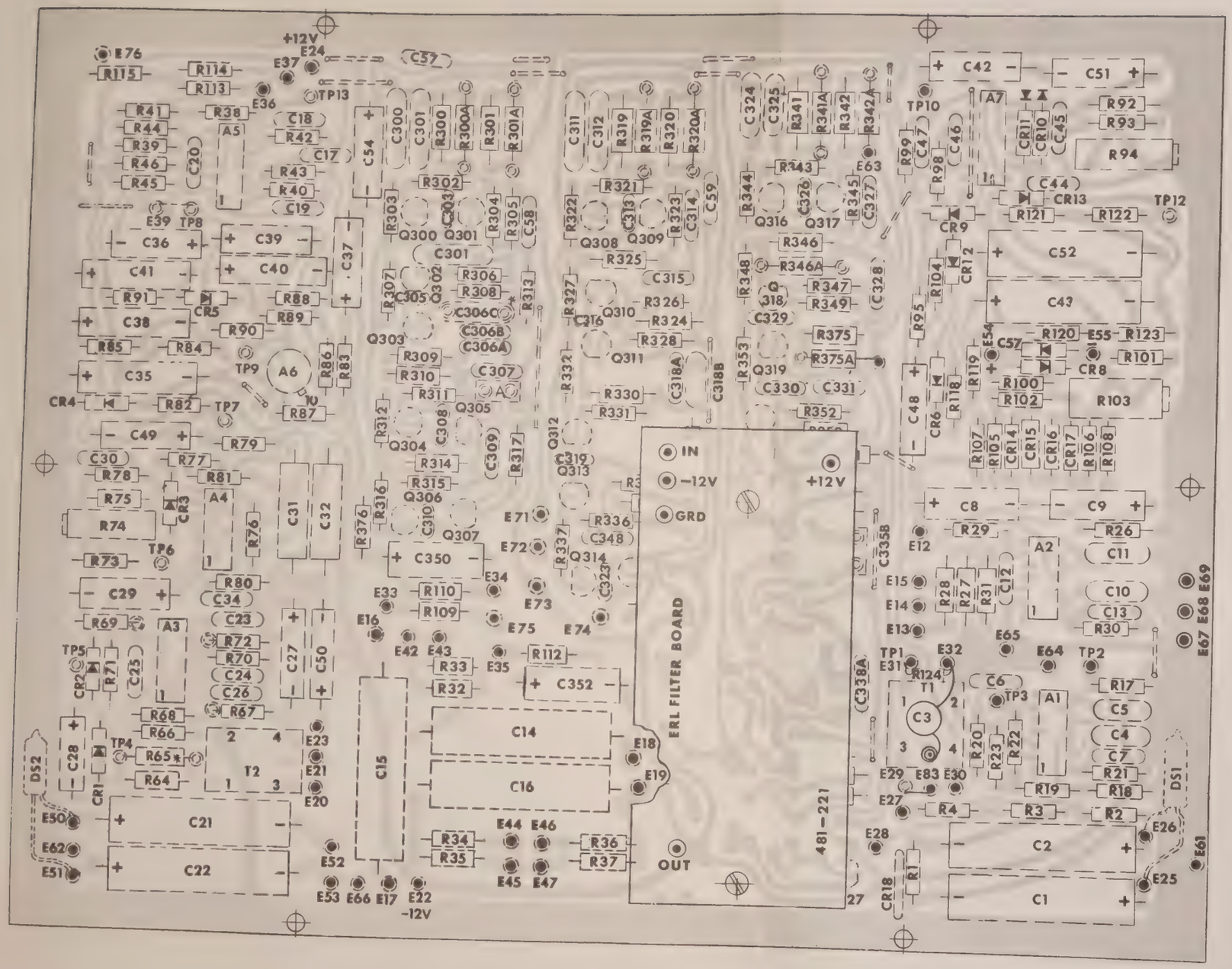
Typical CA3000

Top View

Typical CA3047, CA3030
Plastic Dual In-Line

RETURN LOSS
MEASURING SET
KS-20501 L3

MAIN BOARD
Component Side



SEMICONDUCTOR BASING

Bottom View

Typical 2N3904, 2N3906

Bottom View

Typical 2N5138

Bottom View

Typical 2N5135

Bottom View

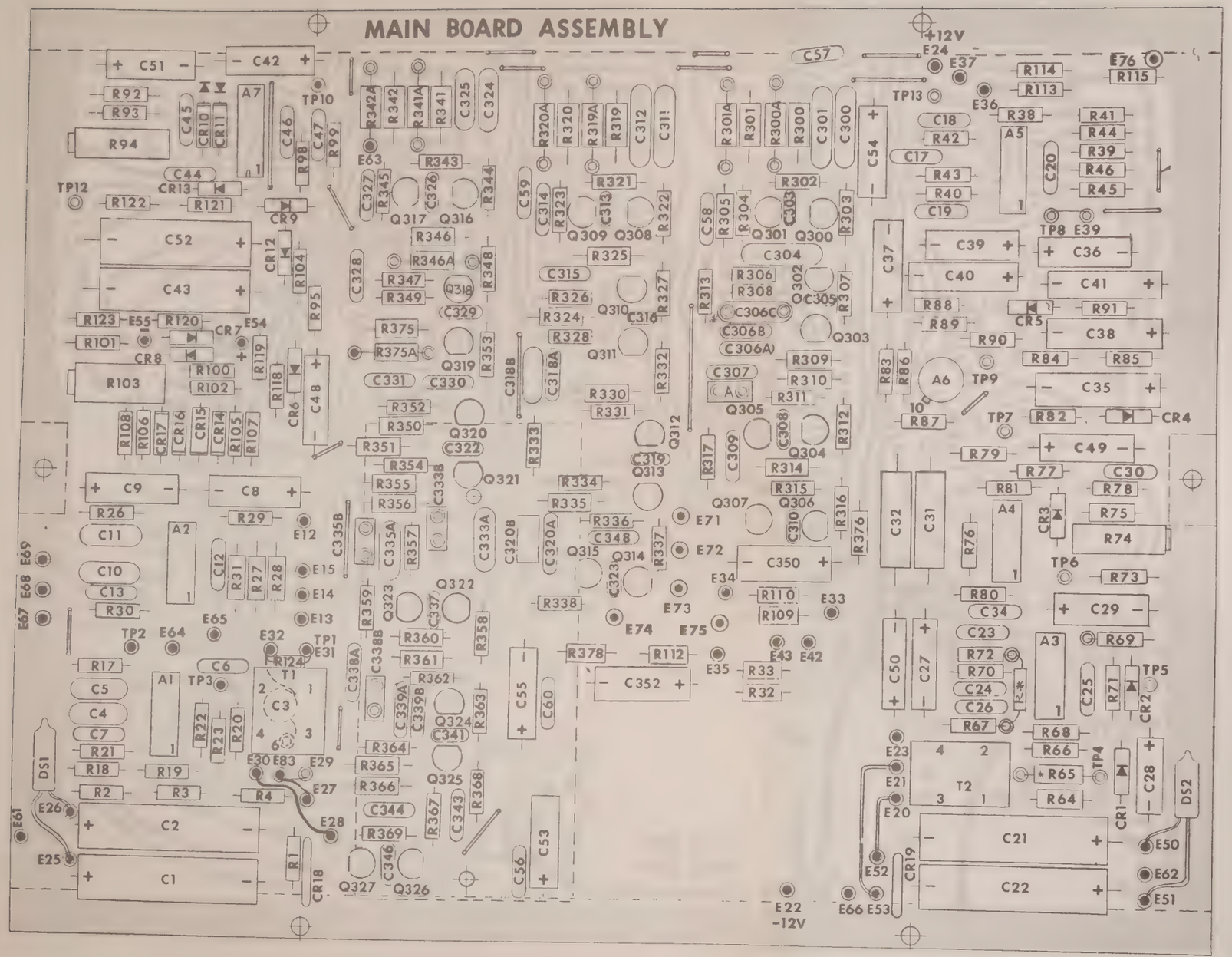
Typical CA3000

Top View

Typical CA3047, CA3030
Plastic Dual In-Line

RETURN LOSS
MEASURING SET
KS-20501 L3

MAIN BOARD
Circuit Side


MAIN BOARD ASSEMBLY
+12V
-12V
C51
C42
C57
C52
C43
C48
C9
C8
C2
C1
C350
C352
C53
C55
C60
C54
C37
C39
C40
C36
C41
C38
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C23
C50
C27
C32
C31
C21
C22
C28
T1
T2
A1
A2
A3
A4
A5
A6
A7
R103
R94
R92
R93
R122
R121
R123
R120
R101
R100
R102
R119
R118
R104
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R4
R3
R2
R1
C1
C2
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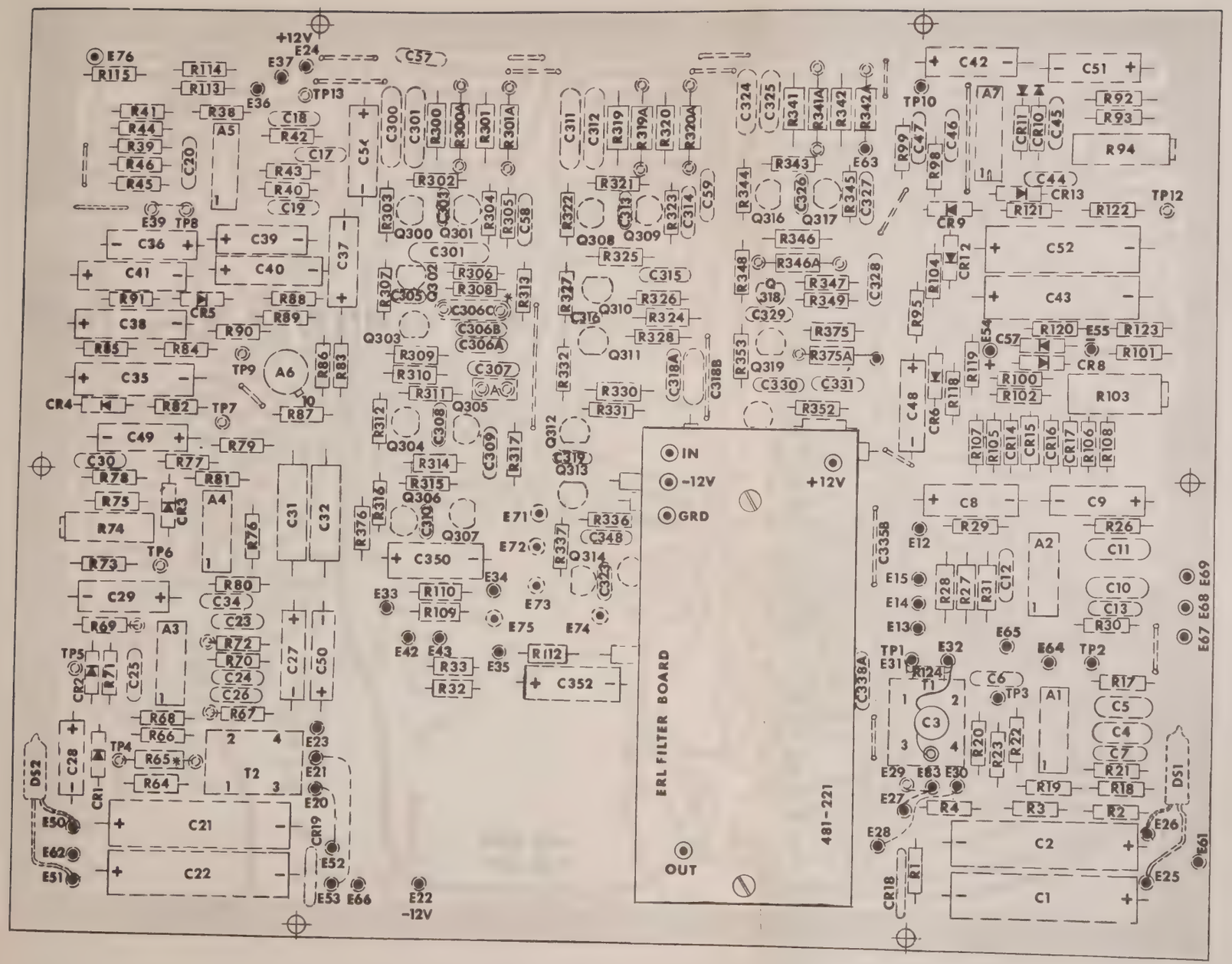


SEMICONDUCTOR BASING

Bottom View

Typical 2N3904, 2N3906

Bottom View

Typical 2N5138

Bottom View

Typical 2N5135

Bottom View

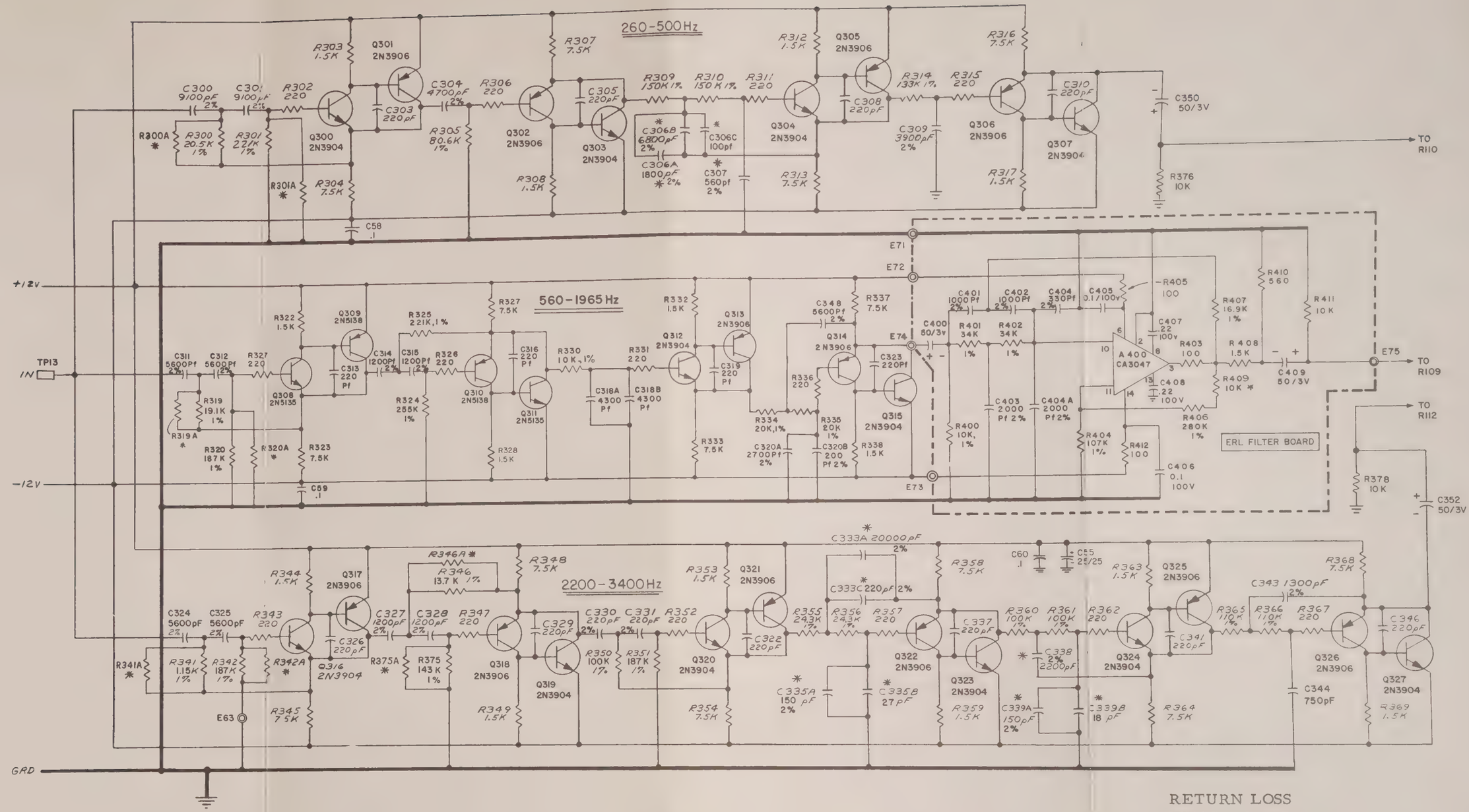
Typical CA3000

Top View

Typical CA3047, CA3030
Plastic Dual In-Line

RETURN LOSS
MEASURING SET
KS-20501 L4

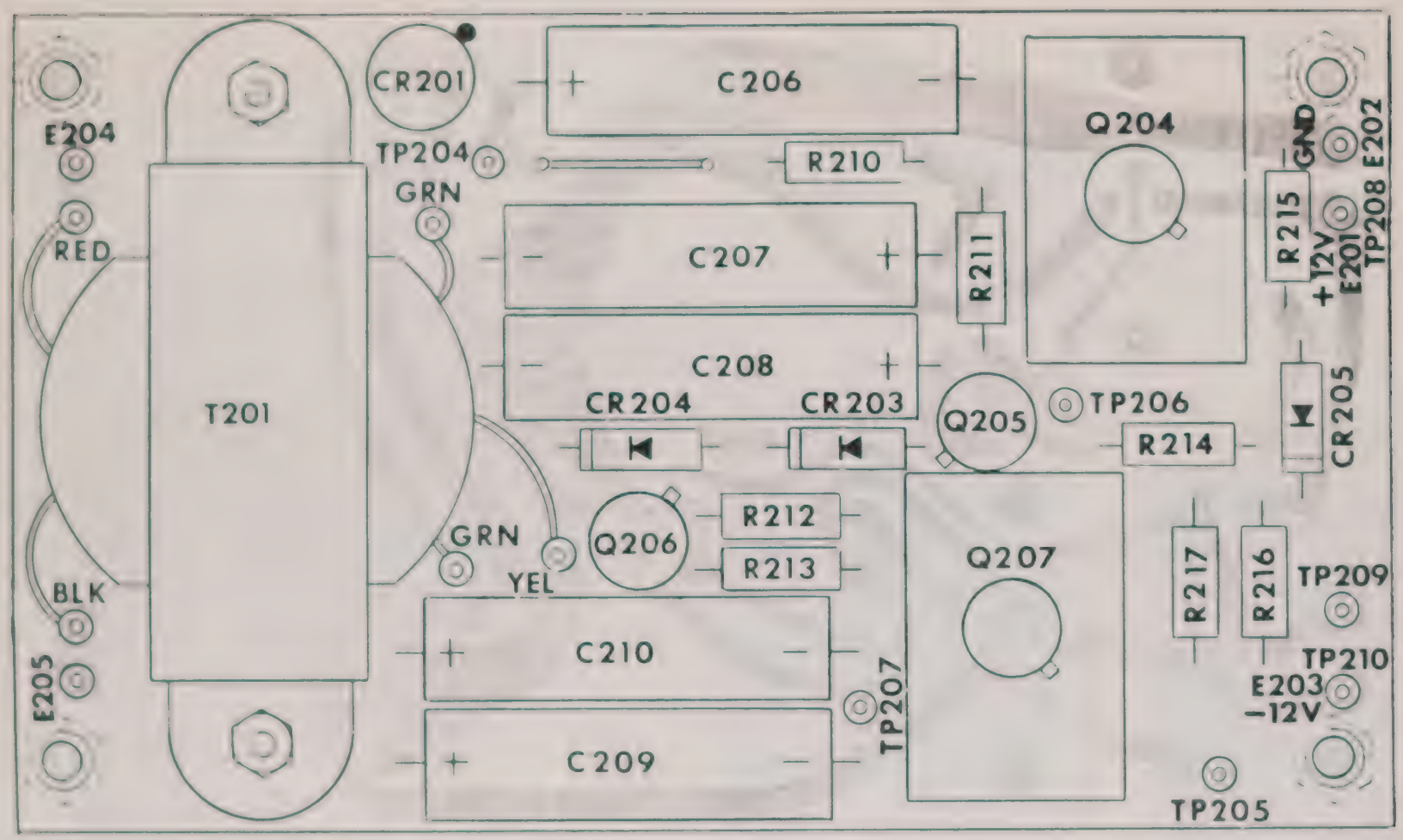
MAIN BOARD
Circuit Side



* Selected components

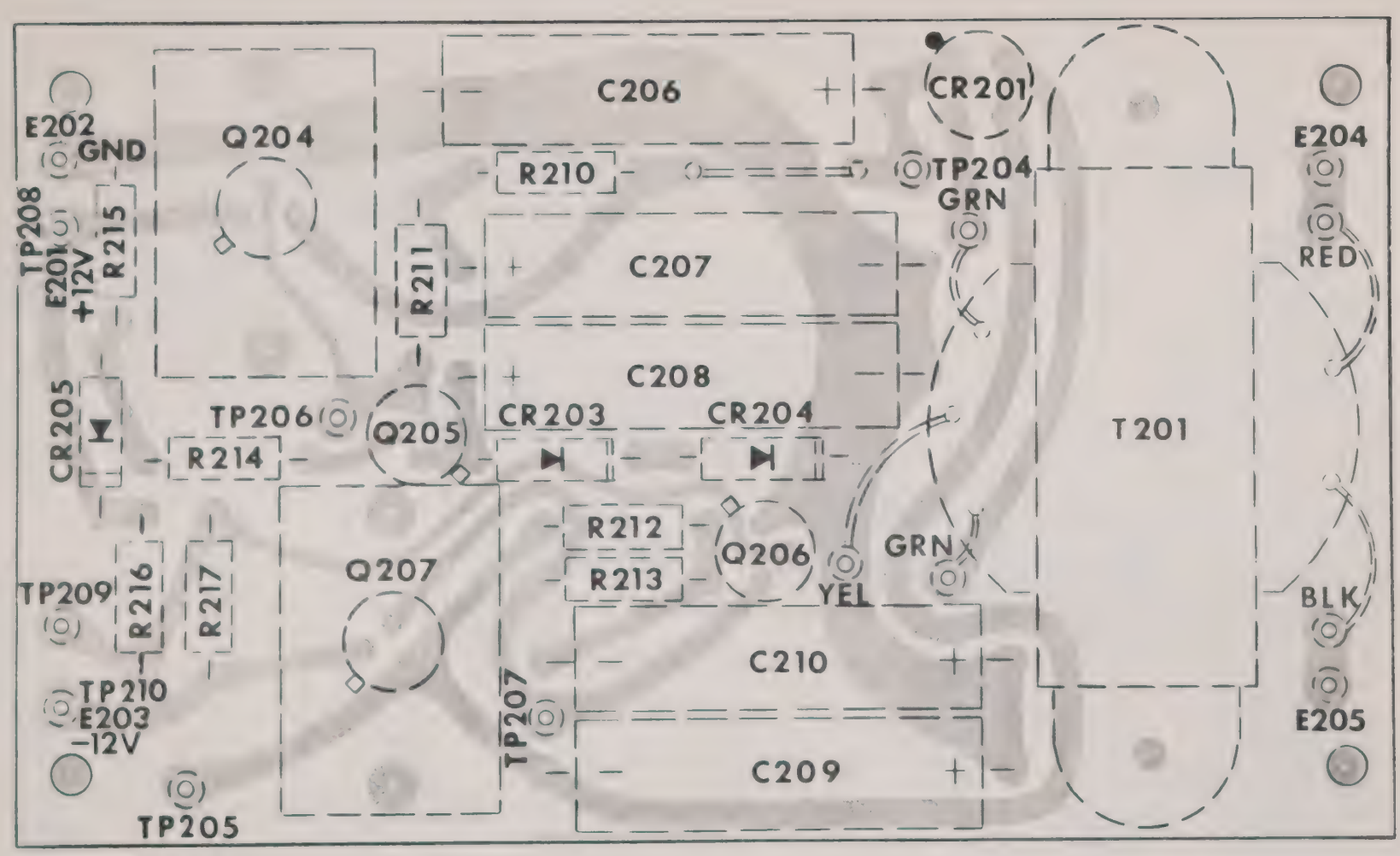
RETURN LOSS
MEASURING SET
KS-20501 L3 and L4

MAIN SCHEMATIC
Filter Section



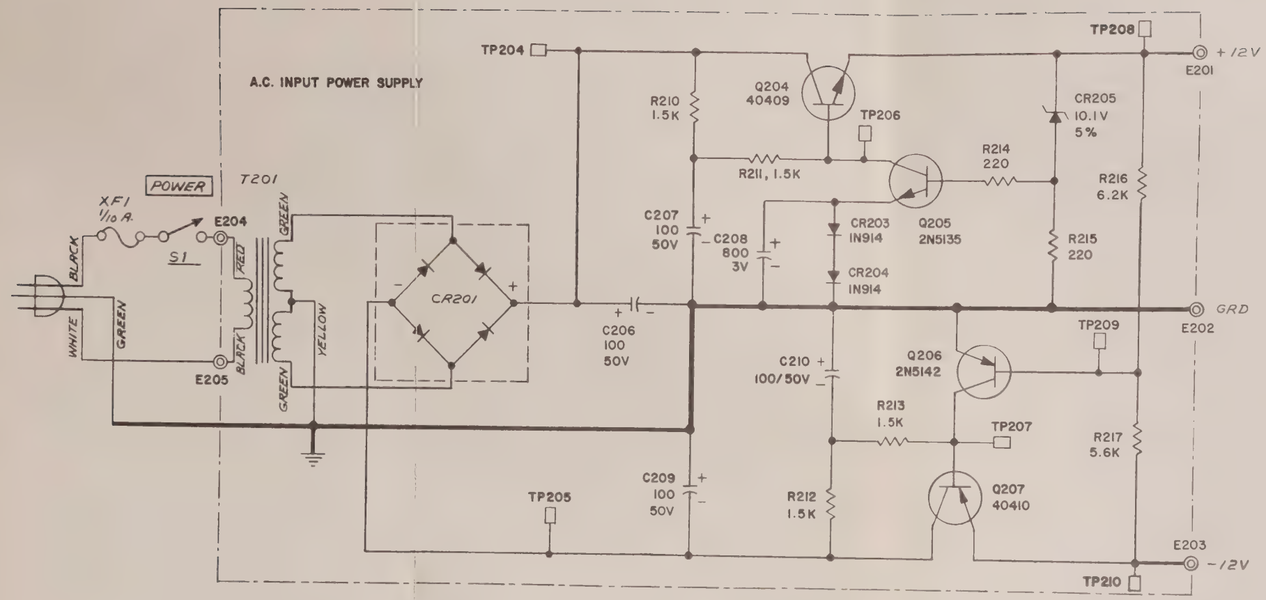
RETURN LOSS MEASURING SET

AC POWER SUPPLY
Component Side



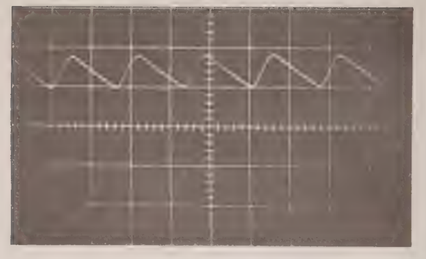
RETURN LOSS MEASURING SET

AC POWER SUPPLY
Circuit Side

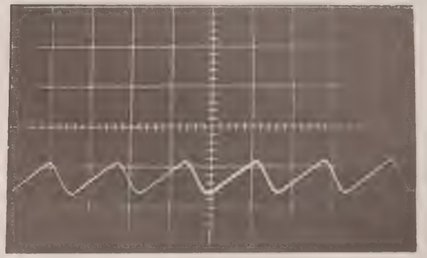


List of Materials - See 7-5 and 7-6

Assembly Drawings - See 6.2.6 and 6.2.7



TP204 Vert= 5V/cm, Hor= 5ms/cm



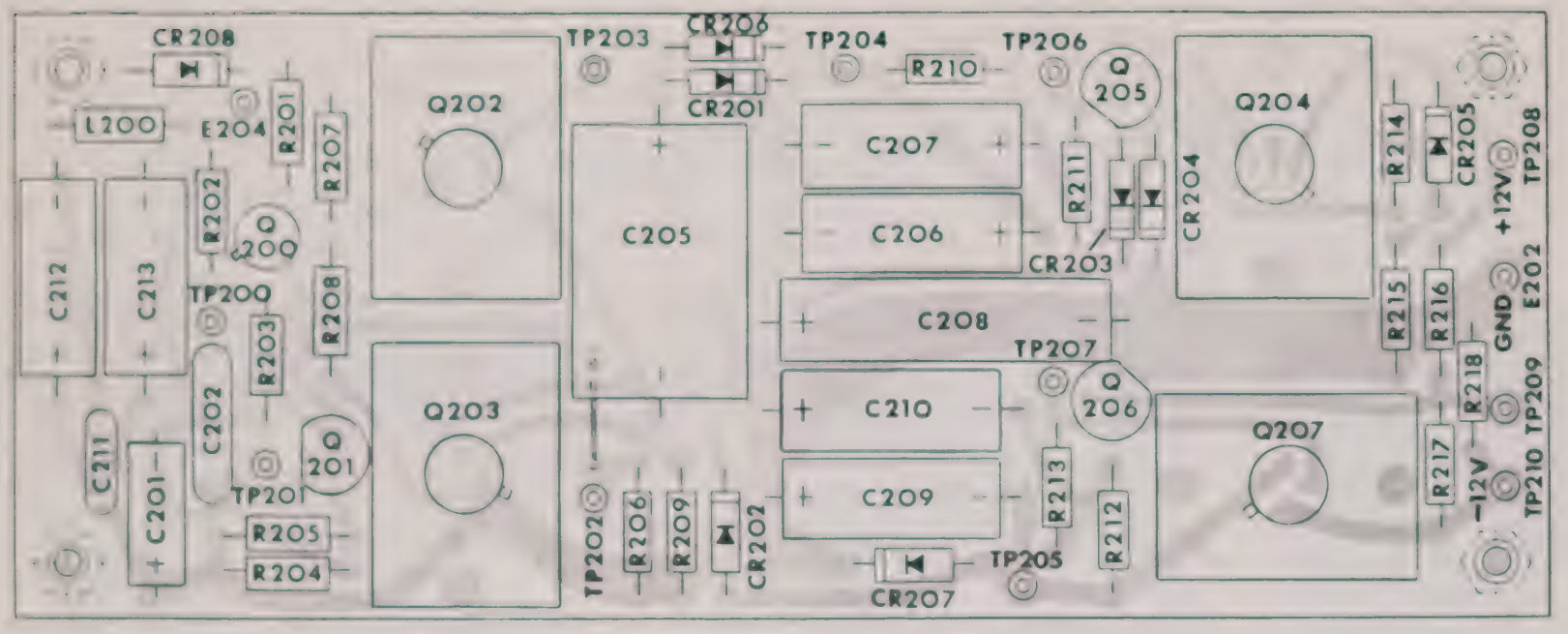
TP205 Vert= 5V/cm, Hor= 5ms/cm

Typical Voltages

TP	VDC	VAC
204	+25.70	-
205	-25.30	-
206	+12.90	-
207	-12.70	-
208	+12.20	0.0008
209	+ 0.60	-
210	-12.00	0.0006

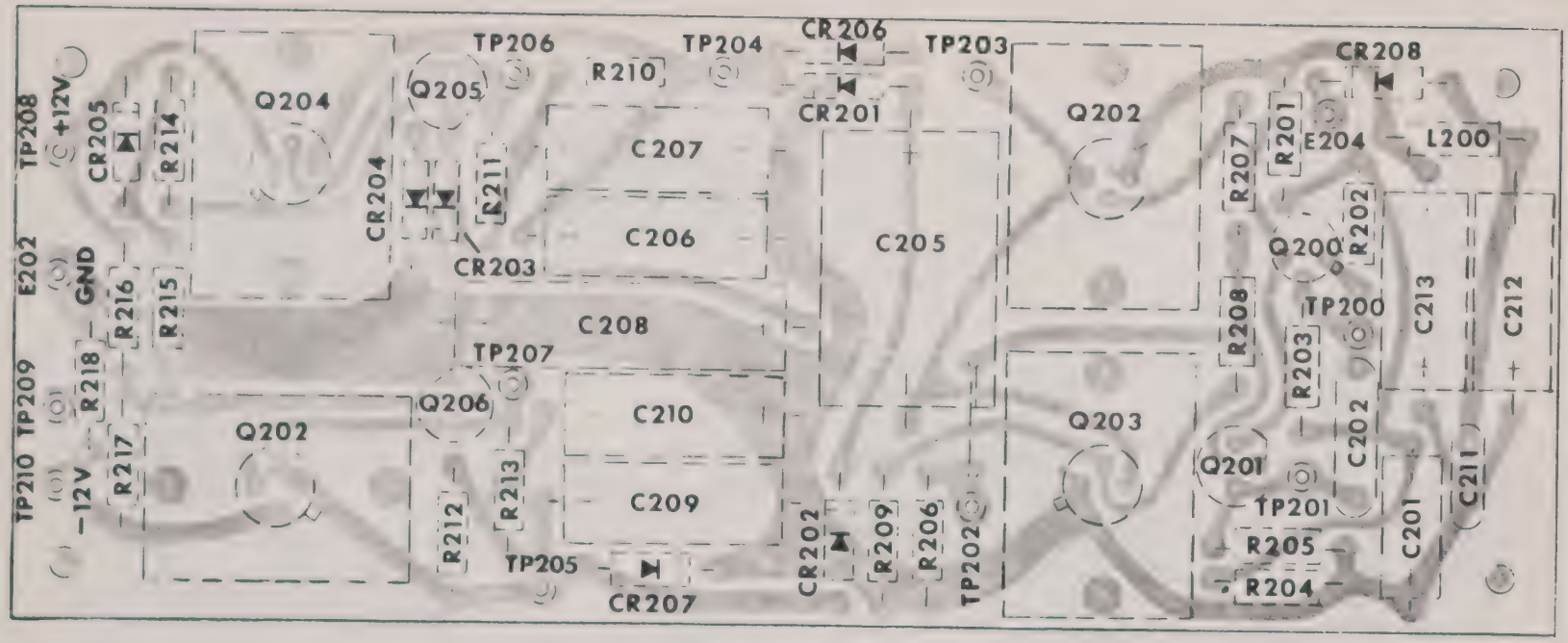
RETURN LOSS
MEASURING SET
KS-20501 L3

AC POWER SUPPLY
Schematic



RETURN LOSS MEASURING SET

DC POWER SUPPLY
Component Side

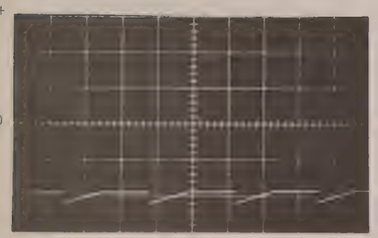


RETURN LOSS MEASURING SET

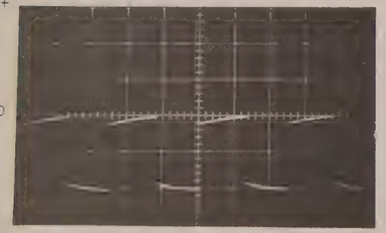
DC POWER SUPPLY
Circuit Side

List of Materials - See 7-6 and 7-7

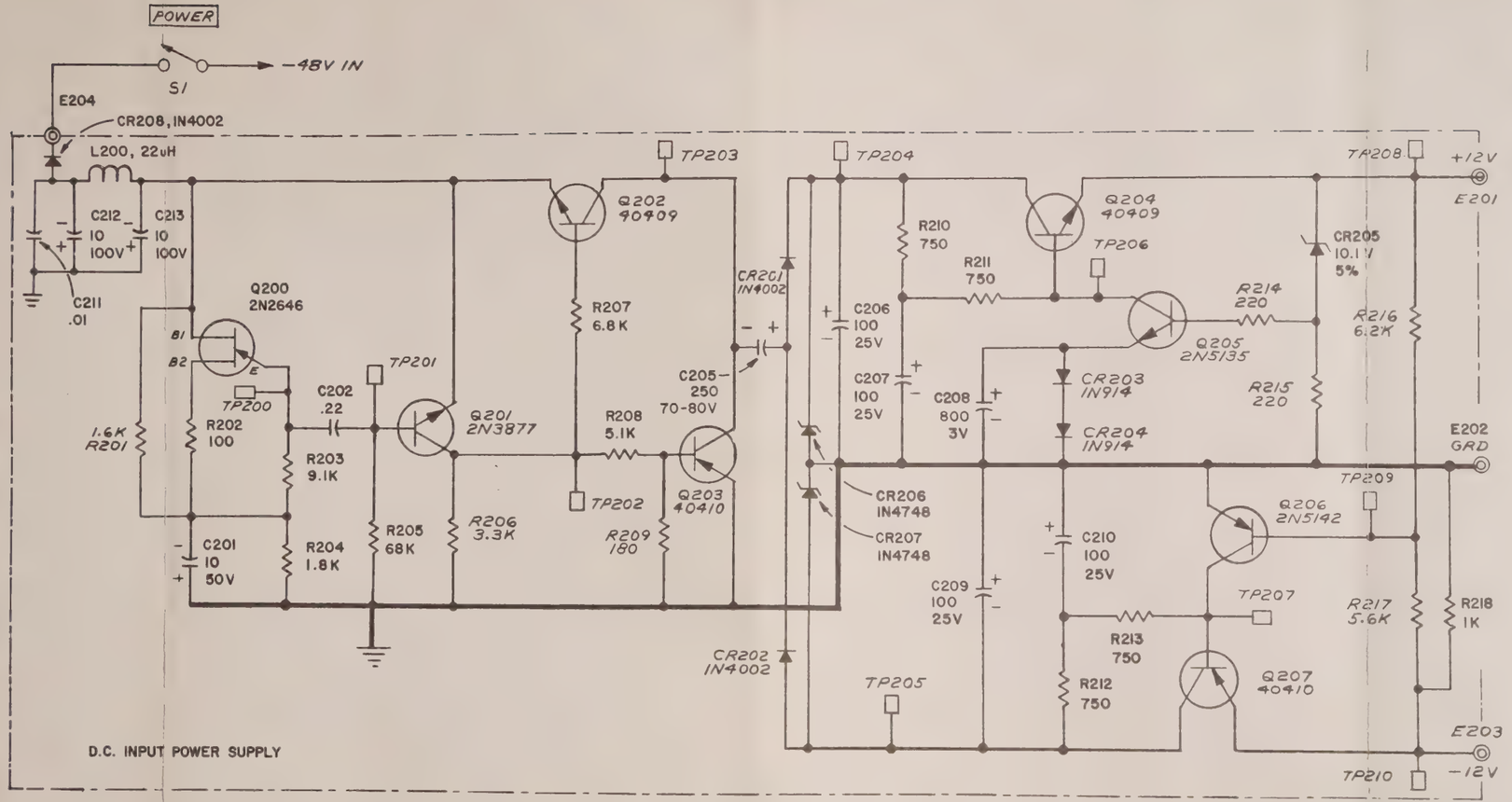
Assembly Drawings - See 6.2.9 and 6.2.10

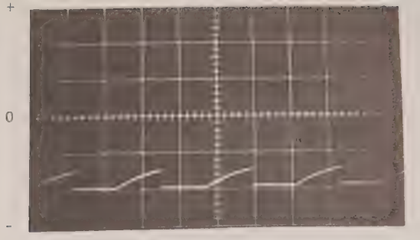


TP201 Vert= 20V/cm, Hor= 2ms/cm

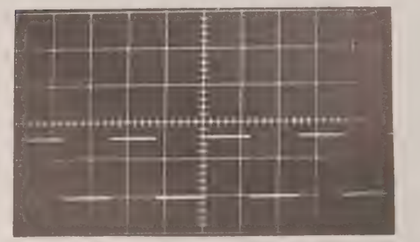


TP203 Vert= 20V/cm, Hor= 2ms/ cm





TP200 Vert= 20V/cm, Hor= 2ms/cm



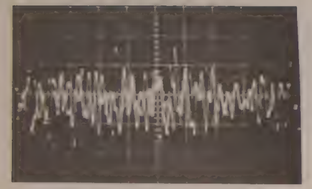
TP202 Vert= 20V/cm, Hor= 2ms/cm

Typical Voltages

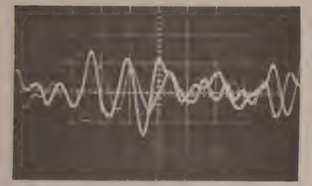
TP	VDC	VAC
204	+25.70	-
205	-25.30	-
206	+12.90	-
207	-12.70	-
208	+12.20	0.0008
209	+ 0.60	-
210	-12.00	0.0006

RETURN LOSS
MEASURING SET
KS-20501 L4

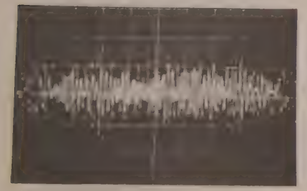
DC POWER SUPPLY
Schematic



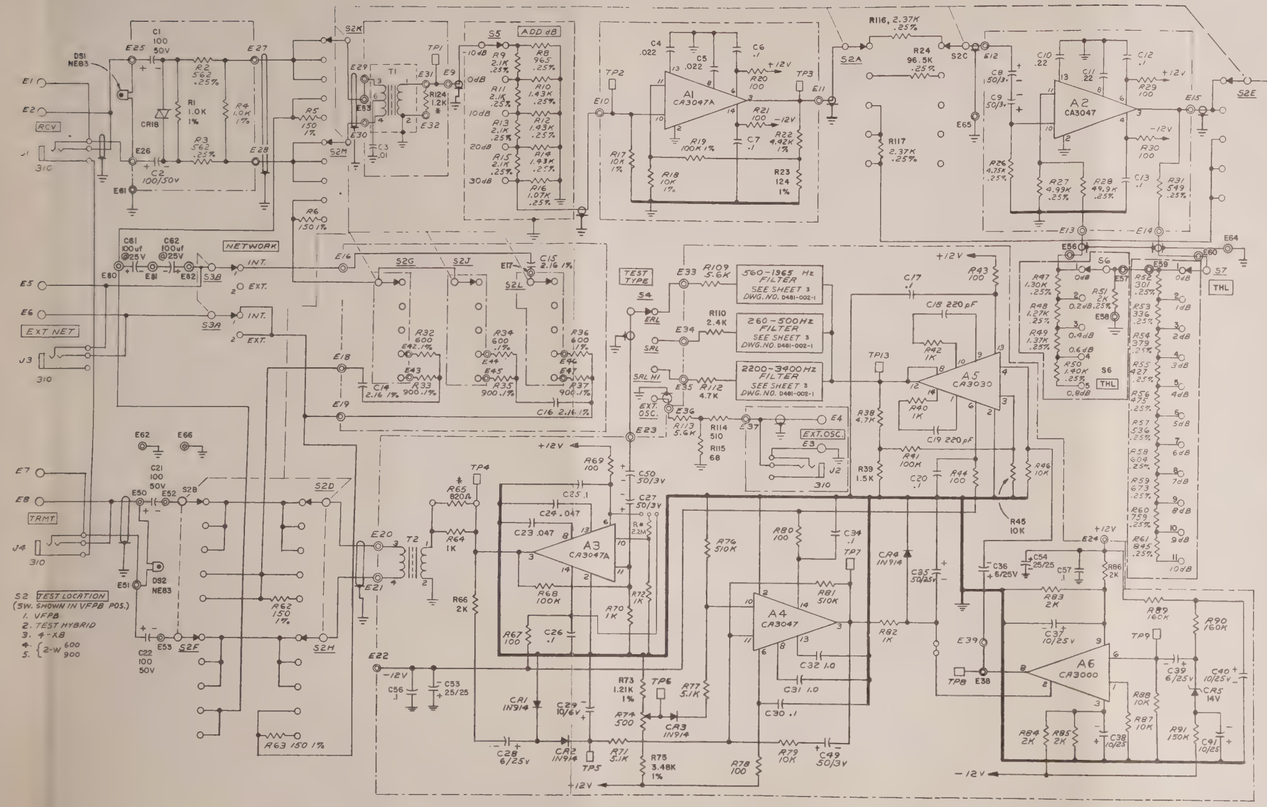
ERL TP4 Vert=2V/cm, Hor=2ms/cm

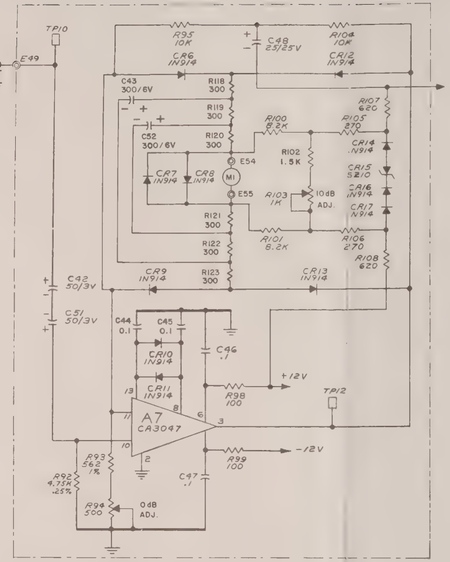


SRL TP4 Vert=2V/cm, Hor=2ms/cm

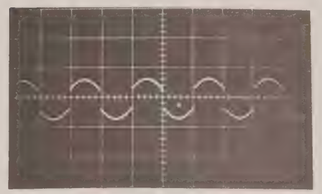


SRL HI TP4 Vert=2V/cm. Hor=2ms/cm





Waveform below taken with input to RCV set at 1 kHz, -3dB level, 600 ohm load, PWR, ON; THL, 0.0; TEST LOCATION, TST HYBRID; TEST TYPE, EXT OSC; ADD dB, 0; NETWORK, INT.



TP12 Vert=10V/cm, Hor=0.5ms/cm

Typical Voltages

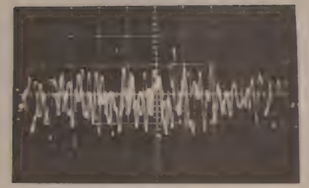
TP	VDC	VAC
1	ac only	1.02
2	0.0	0.003
3	-1.58	1.3
4	-0.1	1.1
5	+3.50	-
6	+3.4	-
7	+9.2	-
8	+3.9	0.05
9	-0.08	0.02
10	-0.14	0.02
13	-0.03	1.02

List of Materials - See 7-2, 7-3, 7-4, 7-5

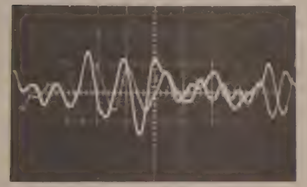
Assembly Drawings - See 6.2.1 and 6.2.2

RETURN LOSS
MEASURING SET
KS-20501 L3

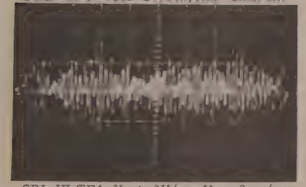
MAIN SCHEMATIC



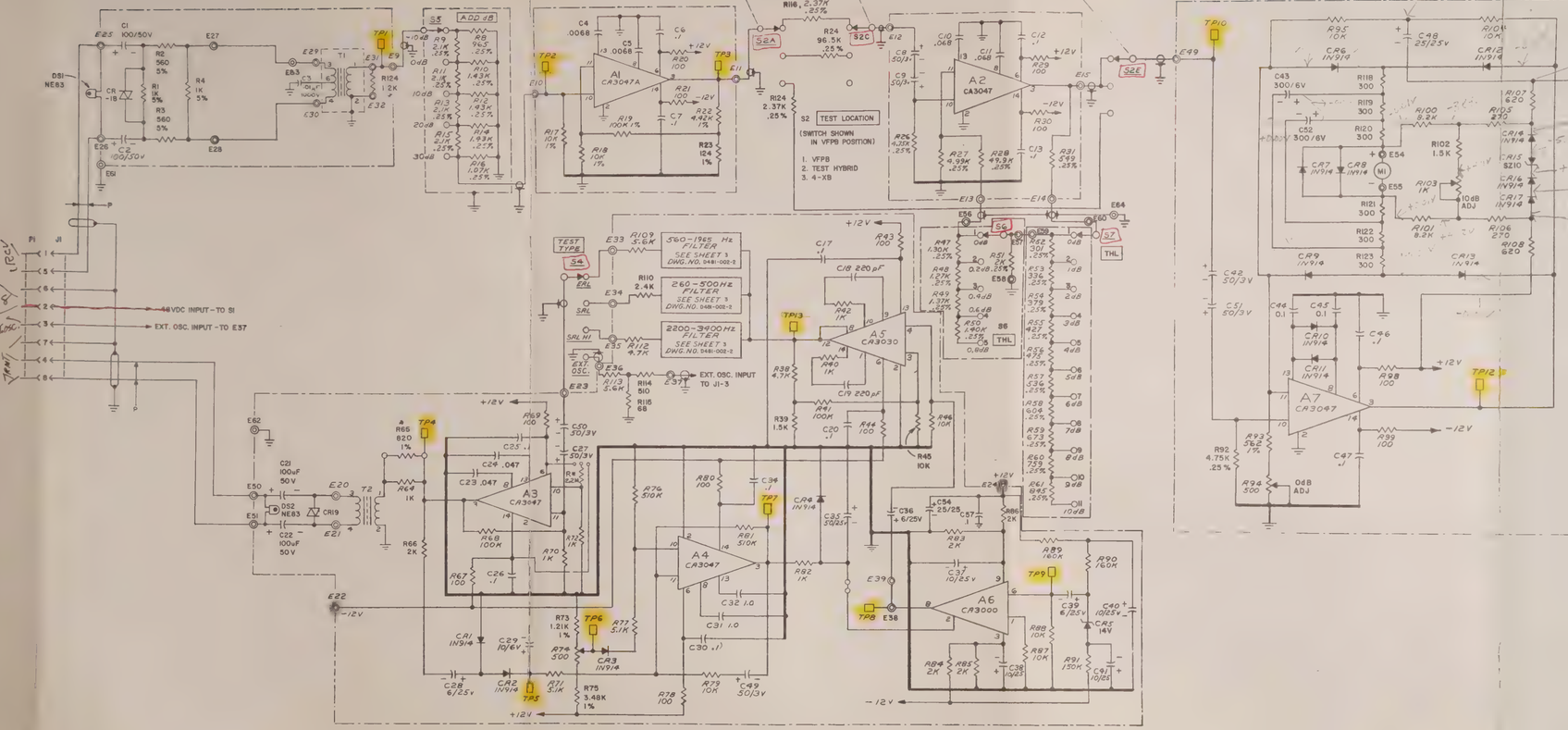
ERL TP4 Vert=2V/cm, Hor=2ms/cm



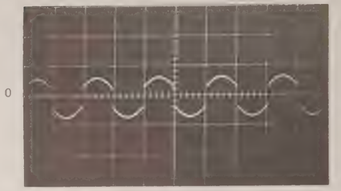
SRL TP4 Vert=2V/cm, Hor=2ms/cm



SRL HI TP4 Vert=2V/cm, Hor=2ms/cm



Waveform below taken with input to RCV set at 1 kHz, -3dB level, 600 ohm load. PWR, ON; THL, 0.0; TEST LOCATION, TST HYBRID; TEST TYPE, EXT OSC; ADD dB, 0.



TP12 Vert=10V/cm, Hor=0.5ms/cm

Typical Voltages

TP	VDC	VAC	
1	ac only	1.02	
2	0.0	0.003	
3	- 1.58	1.3	1.3
4	- 0.1	1.1	
5	+ 3.50	-	
6	+ 3.4	-	
7	+ 9.2	-	
8	+ 3.9	0.05	.022
9	- 0.08	0.02	.006
10	- 0.14	0.02	.006
13	- 0.03	1.02	

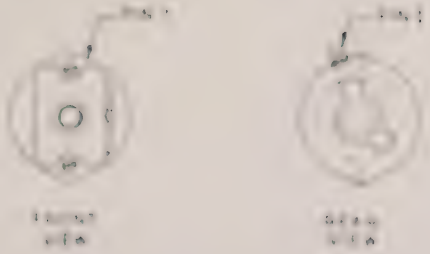
List of Materials - See 7-2, 7-3, 7-4, 7-5

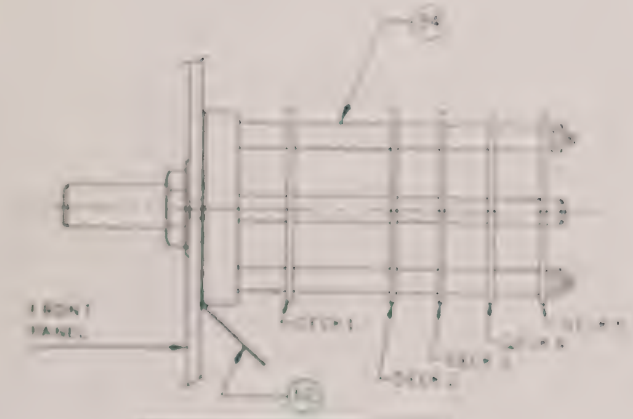
Assembly Drawings - See 6.2. 3 and 6.2.4

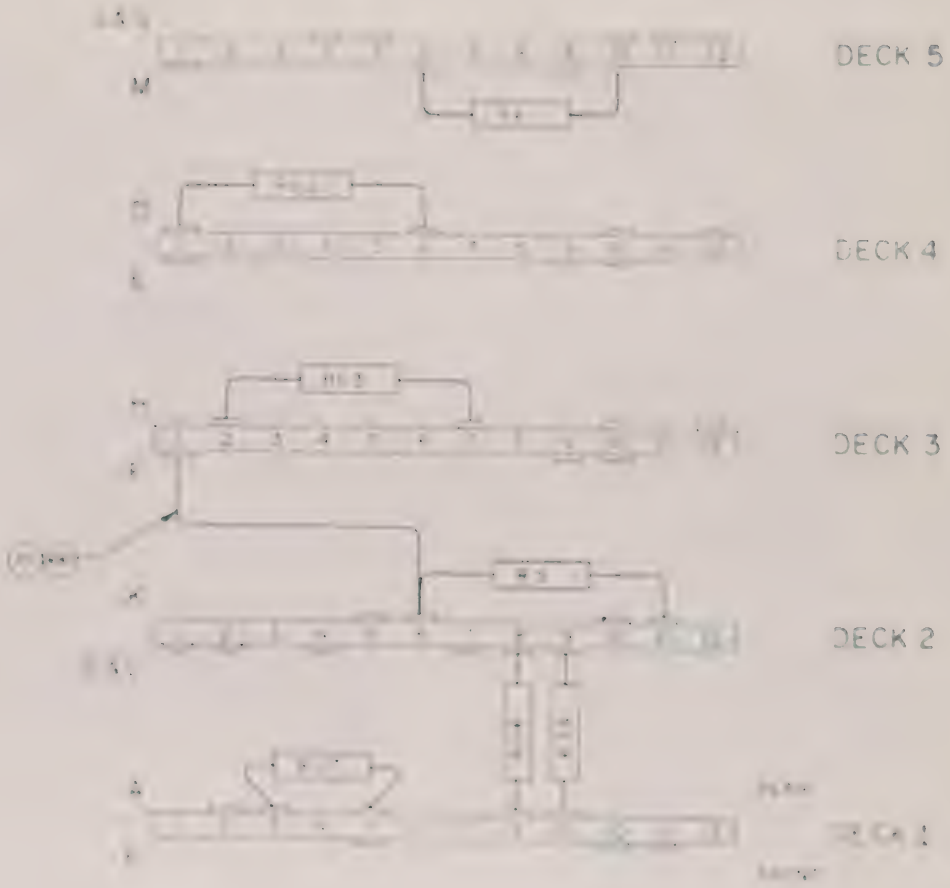
RETURN LOSS
MEASURING SET
KS-20501 L4

MAIN SCHEMATIC

6. 2. 13

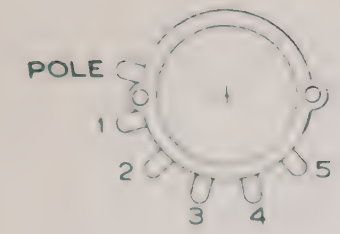


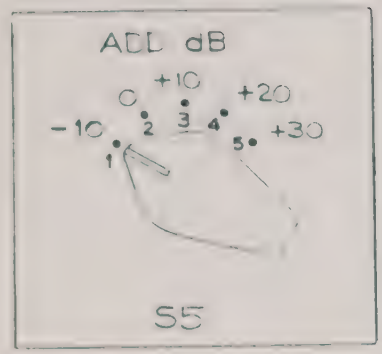


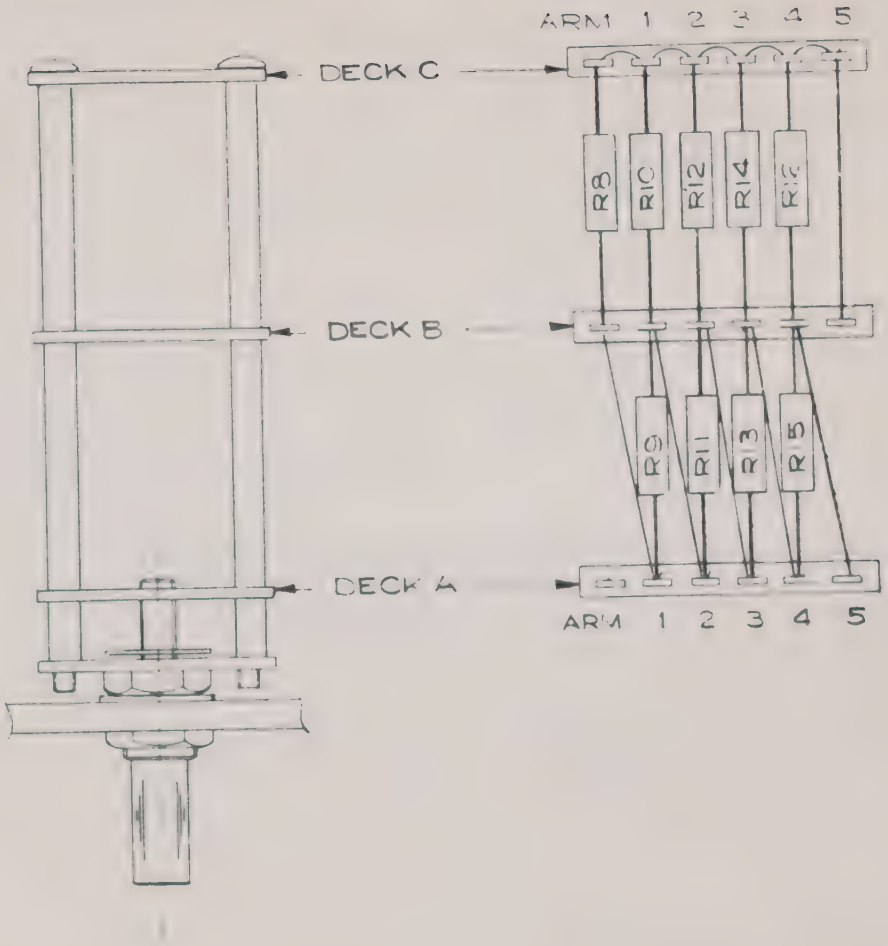


RETURN LOSS MEASURING SET
Switch Detail Test Location
I 3 and I 4

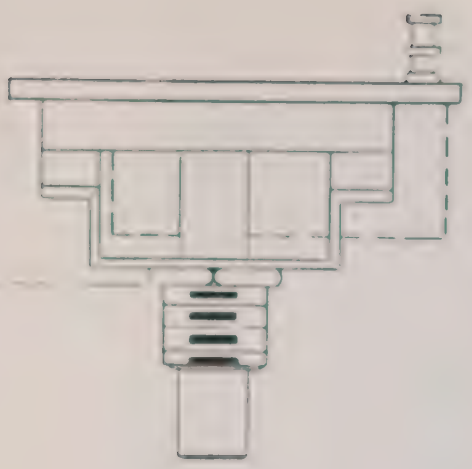
6.2.14

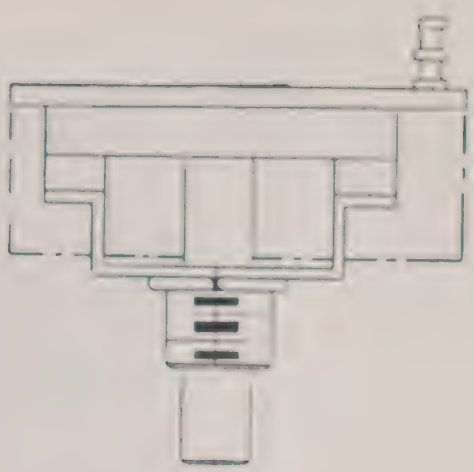


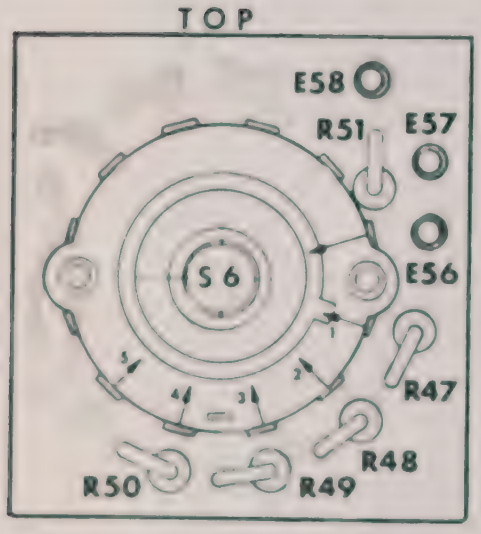




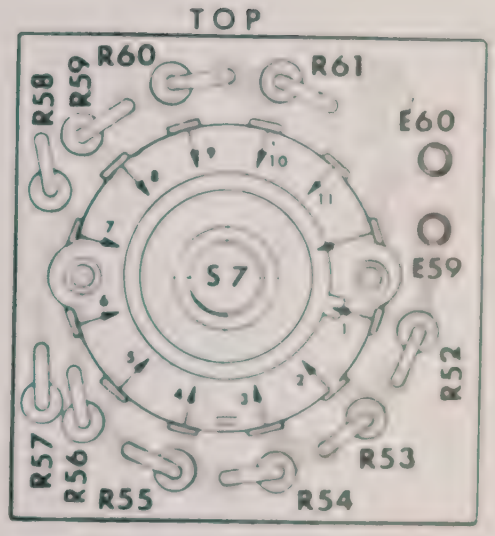
RETURN LOSS MEASURING SET
Switch Detail Add dB
L3 and L4







COMPONENT SIDE
(S6) THL ATTENUATOR
ASSEMBLY

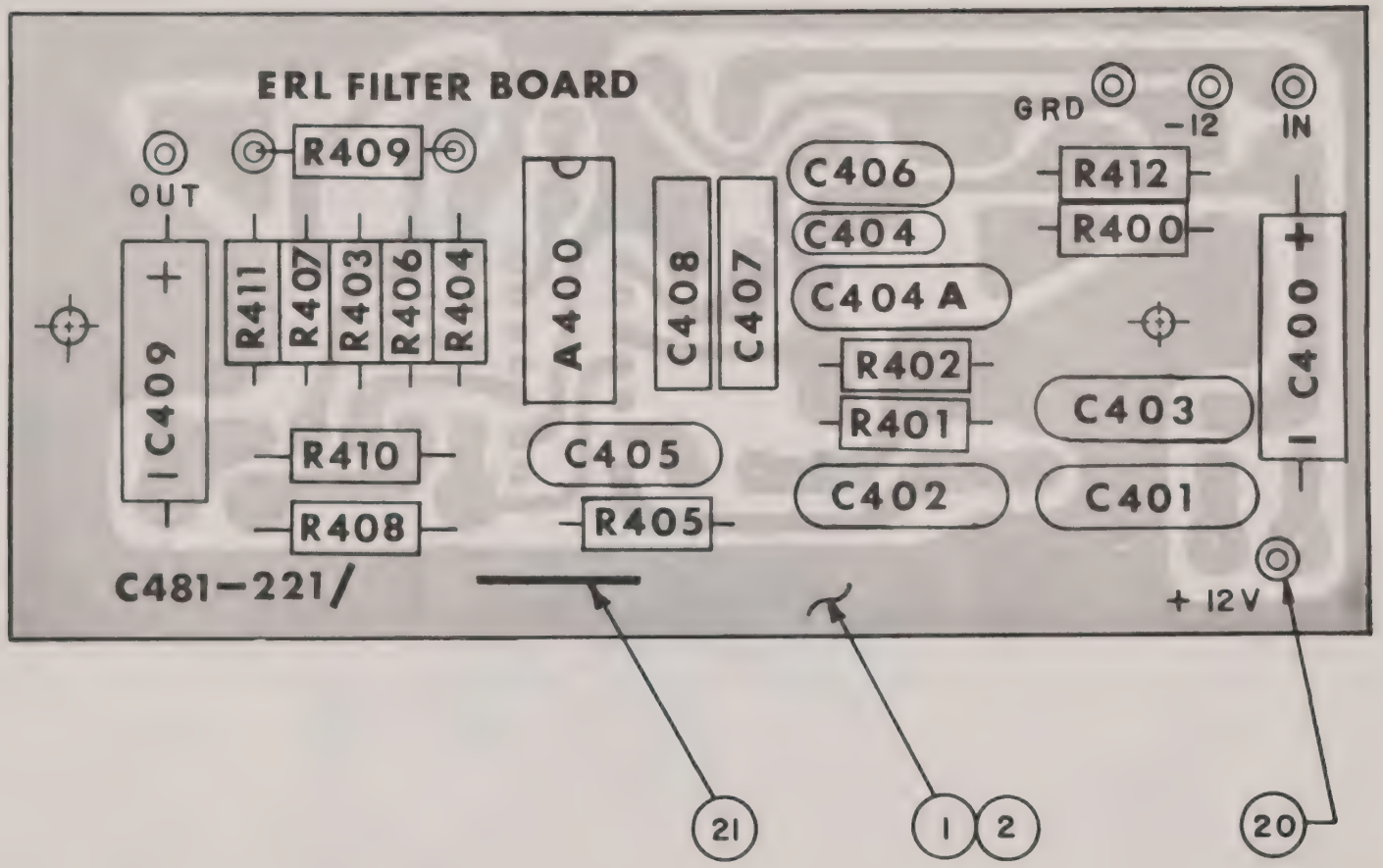


COMPONENT SIDE
(S7) THL ATTENUATOR
ASSEMBLY

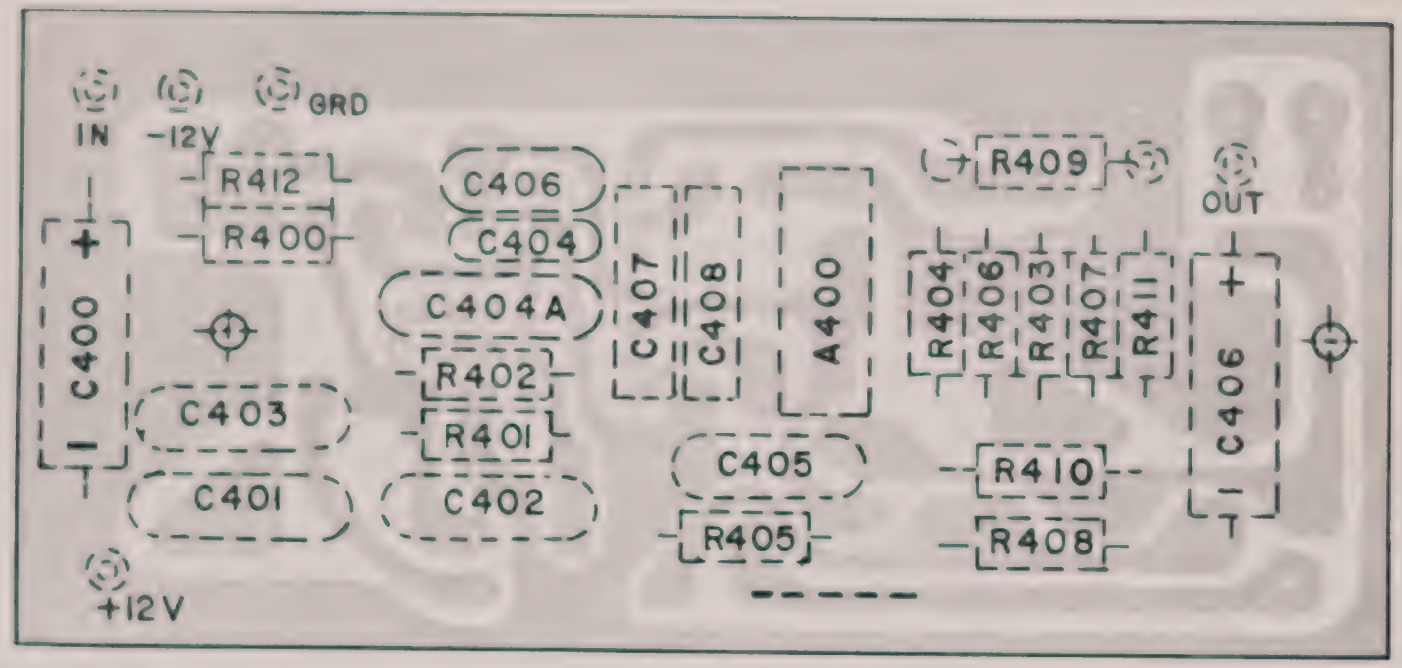
THL
ATTENUATORS

RETURN LOSS MEASURING SET
Switch Detail THL Attenuator
L3 and L4

6.2.16



ERL Filter Board - Component Side



ERL Filter Board - Circuit Side

7.0 PARTS LIST

7.1 General

The parts list itemizes all electrical parts by circuit number. Certain hardware items, such as screws, washers, etc., are not included as these are identifiable and readily available. Generally, the manufacturer's name has been included; however, where the item is a standardized RETMA part, no manufacturer is designated and the product of a registered manufacturer should be acceptable.

Certain items within this parts list may have Bowmar/ALI (ALI) part numbers although they are not manufactured by Bowmar/ALI; these items are purchased to the ALI specification control drawing, as indicated in the parts list.

○ designates those parts found only in the L3 Set.

□ designates those parts found only in the L4 Set.

SYMBOL NUMBER	COMPONENT DESCRIPTION	COMPONENT MANUFACTURER	PART NUMBER
MAIN BOARD - 6.2.1, 6.2.3 (Filter Schematic - 6.2.12, 6.2.13)			
A1, 3	Integrated Circuit	RCA	CA3047A
A2, 4, 7	Integrated Circuit	RCA	CA3047
A5	Integrated Circuit	RCA	CA3030
A6	Integrated Circuit	RCA	CA3000
C1, 2, 21, 22	Capacitor, electrolytic, 100 µF, 50V	Sprague	30D107G050DH4
C3	Capacitor, disc., .01 µF, 20%		CK63AW103M
C4, 5	Capacitor, polyester, .022 µF, 250 V, 10%	Amperex	C280AEA22K
C6, 7, 12, 13, 17, 20, 25, 26, 30, 34, 46, 47, 56, 57, 58, 59, 60	Capacitor, .1 µF, 20 V	Centralab	UK20-104
C8, 9, 27, 42, 49, 50, 51, 350, 352	Capacitor, electrolytic, 50 µF, 10 V	Sprague	TE-1119
C10, 11	Capacitor, polyester, .22 µF, 250 V, 10%	Amperex	C280AE220K
C14, 15, 16	Capacitor, polyester, 2.16 µF, 1%	ALI	C5731-
C18, 19	Capacitor, mica, 220 pf, 500 V, 5%	CDE	CM05FD221J03
C23, 24	Capacitor, .047 µF, 250 V	Amperex	C280AEA47K
C28, 36, 39	Capacitor, electrolytic, 6 µF, 25 V	Sprague	TE-1203
C29	Capacitor, electrolytic, 10 µF, 6 V	Sprague	TE-1087
C31, 32	Capacitor, polyester, 1.0 µF, 200 V, 10%	Amperex	C280AE/AIM
C35	Capacitor, electrolytic, 50 µF, 25 V	Sprague	TE-1209
C37, 38, 40, 41	Capacitor, electrolytic, 10 µF, 25 V	Sprague	TE-1204
C43, 52	Capacitor, electrolytic, 300 µF, 6 V	Sprague	TE-1106
C44, 45	Capacitor, polyester, .1 µF, 250 V, 10%	Amperex	C280AEA100K
C48	Capacitor, electrolytic, 25 µF, 25 V	Sprague	TE-1207
C53, 54, 55	Capacitor, 25 µF, 25 V	Ducati	25 DUM 25
C300, 301	Capacitor, mica, 9100 pF, 500 V, 2%	CDE	CD30ED912G03
C303, 305, 308, 310, 313, 316, 319, 322, 323, 326, 329, 337, 341, 346	Capacitor, mica, 220 pF, 600 V, 10%	Centralab	DD221
C304	Capacitor, mica, 4700 pF, 500 V, 2%	CDE	CD19ED472G03
C306A	Capacitor, mica, 1800 pF, 500 V, 2%	CDE	CD19ED182G03
C306B	Capacitor, mica, 6800 pF, 500V, 2%	CDE	CD30ED682G03
C306C	Capacitor, mica, 100 pF, 500 V, 2%	CDE	CD10ED101G03
C318A, 318B	Capacitor, mica, 4300 pF, 2%	CDE	CD19FD432G03
C338B	Capacitor, mica, 33 pF, 500 V, 5%	CDE	CM04ED330J03
C307A	Capacitor, mica, 62 pF, 500 V, 5%	CDE	CM04ED620J03

C345	Capacitor, mica, 5600 pF, 500 V, 2%	CDE	CD30ED562G03
C307	Capacitor, mica, 560 pF, 500 V, 2%	CDE	CD19ED561G03
C309	Capacitor, mica, 3900 pF, 500 V, 2%	CDE	CD19ED392G03
C311, 312, 324, 325, 348	Capacitor, mica, 5600 pF, 500 V, 2%	CDE	CD19ED562G03
C314, 315, 327, 328	Capacitor, mica, 1200 pF, 500 V, 2%	CDE	CD19ED122G03
C330, 331, 330	Capacitor, mica, 220 pF, 500 V 2%	CDE	CD10ED221G03
C335B	Capacitor, mica, 27 pF, 500 V, 5%	CDE	CD15ED270J03
C320A	Capacitor, mica, 2700 pF, 500 V, 2%	CDE	CD19ED272G03
C320B	Capacitor, mica, 200 pF, 500 V, 2%	CDE	CM06FD201J03
C333A	Capacitor, mica, 20,000 pF, 500 V, 2%	CDE	CD30ED203G03
C335A, 339A	Capacitor, mica, 150 pF, 500 V, 2%	CDE	CD15ED151G03
C338, 333B	Capacitor, mica, 2200 pF, 500 V, 2%	CDE	CD19FD222G03
C339B	Capacitor, mica, 18 pF, 500 V, 5%	CDE	CD10ED180J03
C343	Capacitor, mica, 1300 pF, 500 V, 2%	CDE	CD19ED132G03
C344	Capacitor, mica, 750 pF, 500 V, 2%	CDE	CD19ED751G03
CR1, 2, 3, 4, 6, 7, 8, 9, 10, 11, 12, 13, 14, 16, 17	Diode		IN914
CR5	Diode, Zener, noise generator	Solitron	SD10W/24
CR15	Diode, Zener, 10 V	Schauer	SZ10
CR18, 19	Varistor (GE) V130LA10A	VECO	063L4
DS1, 2	Lamp, circuit glow	Chicago Miniature	NE83
Q300, 303, 304, 307, 308, 311, 312, 315, 316, 319, 320, 323, 324, 327	Transistor		MPS3904 or 2N3904
Q301, 302, 305, 306, 309, 310, 313, 314, 317, 318, 321, 325, 326, 332	Transistor		MPS3906 or 2N3906
R1, 4	Resistor, 1.00 K, 1/8 W, 1%		RN60C1001F
R2, 5	Resistor, 562 Ω, 1/8 W, .25%		RN60C5620C
R3, 11	Resistor, 560 Ω, 1/4 W, 5%		RC07GF561J
R17, 18, 330, 376, 378	Resistor, 10.0 K, 1/8 W, 1%		RN60C1002F
R19, 350, 360, 361	Resistor, 100 K, 1/8 W, 1%		RN60C1003F
R20, 21, 29, 30, 43, 44, 67, 69, 78, 80, 98, 99	Resistor, 100 Ω, 1/4 W, 5%		RC07GF101J
R334, 338	Resistor, 20 KΩ, 1/8 W, 1%		RN60C2002C
R301A	Resistor, 2.7 M, 1/4 W, 5%		RC07GF275J

R22	Resistor, 4.42 K, 1/8 W, 1%		RN60C4421F
R23	Resistor, 124 Ω, 1/8 W, 1%		RN60C1240F
R26, 92	Resistor, 4.75 K, 1/8 W, .25%		RN60C4751C
R27	Resistor, 4.99 K, 1/8 W, .25%		RN60C4991C
R28	Resistor, 49.9 K, 1/8 W, .25%		RN60C4492C
R31	Resistor, 549 Ω, 1/8 W, .25%		RN60C5490C
R32, 34, 36	Resistor, 600 Ω, 1/8 W, 0.1%		RN65C6000B
R33, 35, 37	Resistor, 900 Ω, 1/8 W, 0.1%		RN65C9000B
R38, 112	Resistor, 4.7 K, 1/4 W, 5%		RC07GF472J
R39, 303, 308, 312, 317, 322, 328, 332, 338, 344, 349, 353, 359, 363, 369, 102	Resistor, 1.5 K, 1/4 W, 5%		RC07GF152J
R40, 42, 64, 70, 72, 82, 14	Resistor, 1 K, 1/4 W, 5%		RC07GF102J
R41, 68	Resistor, 100 K, 1/4 W, 5%		RC07GF104J
R45, 46, 87, 88, 95, 104, 376, 378	Resistor, 10 K, 1/4 W, 5%		RC07GF103J
R65	Resistor, nominal value, 820 Ω, 1/4 W, 5%		RC07GF820J
R66, 83, 84, 85, 86	Resistor, 2 K, 1/4 W, 5%		RC07GF202J
R71, 77	Resistor, 5.1 K, 1/4 W, 5%		RC07GF512J
R73	Resistor, 1.21 K, 1/8 W, 1%		RN60C1211F
R74, 94	Potentiometer, 500 Ω, 3/4 W	Beckman IRC	77PR500 Type 980-20
R75	Resistor, 3.48 K, 1/8 W, 1%		RN60C3481F
R76, 81	Resistor, 510 K, 1/4 W, 5%		RC07GF514J
R89, 90	Resistor, 160 K, 1/4 W, 5%		RC07GF164J
R91	Resistor, 150 K, 1/4 W, 5%		RC07GF154J
R93	Resistor, 562 Ω, 1/8 W, 1%		RN60C5620F
R100, 101	Resistor, 8.2 K, 1/4 W, 5%		RC07GF822J
R103	Potentiometer, 1 K, 3/4 W	Beckman IRC	77PR1K Type 980-20
R105, 106	Resistor, 270 Ω, 1/4 W, 5%		RC07GF271J
R107, 108	Resistor, 620 Ω, 1/4 W, 5%		RC07GF621J
R109, 113	Resistor, 5.6 K, 1/4 W, 5%		RC07GF562J
R110	Resistor, 2.4 K, 1/4 W, 5%		RC07GF242J
R118, 119, 120, 121, 122, 123	Resistor, 300 Ω, 1/4 W, 5%		RC07GF301J
R114	Resistor, 510Ω, 1/4 W, 5%		RC07GF510J
R314A	Resistor, 43 K, 1/4 W, 5%		RC07GF433J

R342A	Resistor, 620 K, 1/4 W, 5%		RC07GF624J
R114	Resistor, 510 Ω, 1/4 W, 5%		RC07GF511J
R79	Resistor, 20 K, 1/4 W, 5%		RC07GF203J
R115	Resistor, 68 Ω, 1/4 W, 5%		RC07GF680J
R124	Resistor, nominal value, 1.2 K, 1/4 W, 5%		RC07GF122J
R300	Resistor, 20.5 K, 1/8 W, 1%		RN60C2052F
R320, 342, 351, 320A	Resistor, 187 K, 1/8 W, 1%		RN60C1873F
R302, 306, 311, 315, 321, 326, 331, 336, 343, 347, 352, 357, 362, 367	Resistor, 220 Ω, 1/4 W, 5%		RC07GF221J
R304, 307, 313, 316, 323, 327, 333, 337, 345, 348, 354, 358, 364, 368	Resistor, 7.5 K, 1/4 W, 5%		RC07GF752J
R305	Resistor, 80.6 K, 1/8 W, 1%		RN60C8062F
R309, 310	Resistor, 150 K, 1/8 W, 1%		RN60C1503F
R314	Resistor, 133 K, 1/8 W, 1%		RN60C1333F
R319, 319A	Resistor, 19.1 K, 1/8 W, 1%		RN60C1912F
R324	Resistor, 255 K, 1/8 W, 1%		RN60C2553F
R325, 301	Resistor, 221 K, 1/8 W, 1%		RN60C2213F
R341	Resistor, 1.15 K, 1/8 W, 1%		RN60C1151F
R346	Resistor, 13.7 K, 1/8 W, 1%		RN60C1372F
R355, 356	Resistor, 24.3 K, 1/8 W, 1%		RN60C2432F
R365, 366	Resistor, 110 K, 1/8 W, 1%		RN60C1103F
R375	Resistor, 143 K, 1/8 W, 1%		RN60C1433F
T1, 2	Transformer	Aladdin	95-207
R300A, 319A, 341A, 346A, 375A	Resistor, select		

AC POWER SUPPLY - 6.2.6 (Schematic - 6.2.8)

C206, 207, 209, 210	Capacitor, 100 µF, 50 V	Sprague	TE-1309
C208	Capacitor, 800 µF, 3 V	Sprague	500D807G003DH7
CR201	Bridge rectifier	Varo	VE18
CR203, 204	Diode		IN914
CR205	Diode, Zener, 10.1 V, 5%	Schauer	SZ10
Q204	Transistor	RCA	40409
Q205	Transistor		2N5135
Q206	Transistor		2N5142

Q207	Transistor	RCA	40410
R210, 211, 212, 213	Resistor, 1.5 K, 1/2 W, 5%		RC20GF152J
R214, 215	Resistor, 220 Ω, 1/2 W, 5%		RC20GF221J
R216	Resistor, 6.2 K, 1/2 W, 5%		RC20GF622J
R217	Resistor, 5.6 K, 1/2 W, 5%		RC20GF562J
T201	Transformer, power	Microtran	M8290

DC POWER SUPPLY - 6.2.9 (Schematic - 6.2.11)

C201	Capacitor, 10 μF, 50 V	Siemens	B41313-B7106-2
C202	Capacitor, .22 μF, 250 V	Amperex	C280AEA220K
C205	Capacitor, 250 μF, 70-80 V	Siemens	B41010-F8257-T
C206, 207, 209, 210	Capacitor, 100 μF, 25 V	Sprague	TE-1211
C208	Capacitor, 800 μF, 3 V	Sprague	500D807G003DH7
C211	Capacitor, .01 μF, 1 kV, 20%	Centralab	DD-1032
C212, 213	Capacitor, 10 μF, 100 V	Sprague	TE-1407
CR201, 202, 208	Diode		IN4002
CR203, 204	Diode		IN914
CR205	Diode, Zener, 10.1 V, 5%	Schauer	SZ10
CR206, 207	Diode, Zener		IN4748
L200	Choke, R.F., 22 μH, ±10%	Cambion	2960-44
Q200	Transistor, unijunction	GE	2N2646
Q201	Transistor		2N3877
Q202, 204	Transistor	RCA	40409
Q203, 207	Transistor	RCA	40410
Q205	Transistor		2N5135
Q206	Transistor		2N5142
R201	Resistor, 1.6 K, 1/2 W, 5%		RC20GF162J
R202	Resistor, 100 Ω, 1/2 W, 5%		RC20GF101J
R203	Resistor, 9.1 K, 1/2 W, 5%		RC20GF912J
R204	Resistor, 1.8 K, 1/2 W, 5%		RC20GF182J
R205	Resistor, 68 K, 1/2 W, 5%		RC20GF683J
R206	Resistor, 3.3 K, 1/2 W, 5%		RC20GF332J
R207	Resistor, 6.8 K, 1/2 W, 5%		RC20GF682J
R208	Resistor, 5.1 K, 1/2 W, 5%		RC20GF512J
R209	Resistor, 180 Ω, 1/2 W, 5%		RC20GF181J

R210, 211, 212, 213	Resistor, 750 Ω, 1/2 W, 5%		RC20GF751J
R214, 215	Resistor, 220 Ω, 1/2 W, 5%		RC20GF221J
R216	Resistor, 6.2 K, 1/2 W, 5%		RC20GF622J
R217	Resistor, 5.6 K, 1/2 W, 5%		RC20GF562J
R218	Resistor, 1 K, 1/2 W, 5%		RC20GF102J

FRONT PANEL AND CHASSIS MOUNTED PARTS (Main Schematic - 6.2.12, 6.2.13)

C1, 2	Capacitor, electrolytic, 100 μF, 25 V	Sprague	TE-1211
J1, 2, 3, 4, 5, 6	Binding post, black	General Radio	938-C
J7	Binding post, metal	General Radio	938-P
F1	Fuse, 1/10 A, slow blow, 3 AG	Littelfuse	313.100
J11, 12, 13	Phone jack	[illegible]	MT-332B
M1	Meter, SCD	ALI	C5864
R5, 6, 62, 63	Resistor, 150 Ω, 1/8 W, 1%		RN60C1500F
R8	Resistor, 965 Ω, 1/8 W, .25%		RN60C9650C
R9, 11, 13, 15	Resistor, 2.1 K, 1/8 W, .25%		RN60C2101C
R10, 12, 14	Resistor, 1.43 K, 1/8 W, .25%		RN60C1431C
R16	Resistor, 1.07 K, 1/8 W, .25%		RN60C1071C
R34	Resistor, 96.5 K, 1/8 W, .25%		RN60C9652C
R47	Resistor, 1.30 K, 1/8 W, .25%		RN60C1301C
R48	Resistor, 1.27 K, 1/8 W, .25%		RN60C1271C
R49	Resistor, 1.37 K, 1/8 W, .25%		RN60C1371C
R50	Resistor, 1.40 K, 1/8 W, .25%		RN60C1401C
R51	Resistor, 2 K, 1/8 W, .25%		RN60C2001C
R52	Resistor, 301 Ω, 1/8 W, .25%		RN60C3010C
R53	Resistor, 336 Ω, 1/8 W, .25%		RN60C3360C
R54	Resistor, 379 Ω, 1/8 W, .25%		RN60C3790C
R55	Resistor, 427 Ω, 1/8 W, .25%		RN60C4270C
R56	Resistor, 475 Ω, 1/8 W, .25%		RN60C4750C
R57	Resistor, 536 Ω, 1/8 W, .25%		RN60C5360C
R58	Resistor, 604 Ω, 1/8 W, .25%		RN60C6040C
R59	Resistor, 673 Ω, 1/8 W, .25%		RN60C6730C
R60	Resistor, 759 Ω, 1/8 W, .25%		RN60C7590C
R61	Resistor, 845 Ω, 1/8 W, .25%		RN60C8450C
R116, 117, 118, 119	Resistor, 2.37 K, 1/8 W, .25%		RN60C2371C

S1	Switch, DPDT, toggle	C & K	7101
(S2)	Switch, 12P 5P, rotary	CTS	ALI B5871
[S2]	Switch, 3P 3P, rotary	CTS	ALI B5873
(S3)	Switch, 2P 2P, rotary	CTS	ALI B5872
S4	Switch, 1P 4P, rotary	CTS	ALI B5870
S5	Switch, 1P 5P, rotary	CTS	ALI B5867
S6	Switch, 1P 5P, rotary	CTS	ALI B5868
S7	Switch, 1P 11P, rotary	CTS	ALI B5869
XF1	Fuseholder	Littelfuse	342004

ERL FILTER BOARD - 6.2.17 (Schematic - 6.2.18)

C400, 409	Capacitor, electrolytic, 50 µF, 3 V	Sprague	TE 1058
C401, 402	Capacitor, DSM ± 2%, 1000 pF, 500 V	CDE	CD19FD102G03
C403, 404A	Capacitor, DSM 2000 pF, 500 V, ± 2%	CDE	CD19FD202G03
C404	Capacitor, DSM 330 pF, 500 V, ± 2%	CDE	CD15FD331G03
C405, 406	Capacitor, ceramic 0.1 µF, 250 V, +80-20%	Centralab	UK20-104
C407, 408	Capacitor, polyester, 0.22 µF, 250 V, ± 10%	Amperex	C280AE220K
R401, 402	Resistor, 34.0 K, 1/8 W, ± 1%		RN60C3402F
R400	Resistor, 10.0 K, 1/8 W, ± 1%		RN60C1002F
R407	Resistor, 16.9 K, 1/8 W, ± 1%		RN60C1692F
R404	Resistor, 107 K, 1/8 W, ± 1%		RN60C1073F
R403, 405, 412	Resistor, 100Ω, 1/4 W, ± 5%		RC07GF101J
R408	Resistor, 1.5 K, 1/4 W, ± 5%		RC07GF152J
R406	Resistor, 280 K, 1/8 W, ± 1%		RN60C2803F
R410	Resistor, 560 Ω, 1/4 W, ± 5%		RC07GF561J
R409, 411	Resistor, 10 K, 1/4 W, ± 5%		RC07GF103J
A400	Integrated Circuit	RCA	CA3047

LIST OF MANUFACTURERS

Abbreviation	Complete Name and Address
Aladdin	Aladdin Electronics 701 Murfreesboro Road Nashville, Tennessee 37210 USA
Alco	Alco Electronic Products, Inc. P. O. Box 1348 Lawrence, Massachusetts 01842 USA
ALI	Bowmar/ALI, Inc. 531 Main Street Acton, Massachusetts 01720 USA
Amperex	Amperex Electronics Corporation Component Division 35 Hoffman Avenue Hauppauge, New York 11787 USA
Amphenol	Amphenol Connector Division Bunker-Ramo Corporation 2801 South 25th Avenue Broadview, Illinois 60153 USA
Beckman	Beckman Instruments, Inc. Helipot Division 2500 Harbor Boulevard Fullerton, California 92634 USA
Belden	Belden Corporation P. O. Box 5070-A Chicago, Illinois 60680 USA
Cambion	Cambridge Thermionic Corporation 445 Concord Avenue Cambridge, Massachusetts 02138 USA
CDE	Cornell Dublier Electronics 50 Paris Street Newark, New Jersey 07101 USA
Centralab	Centralab 5757 North Greenbay Avenue Milwaukee, Wisconsin 53209 USA

Chicago Miniature	Chicago Miniature Lamp Works 4433 North Ravenswood Avenue Chicago, Illinois 60640 USA
Circon	Circon Component Corporation Santa Barbara Airport Goleta, California 93017 USA
C & K	C & K Components, Inc. 103 Morse Street Watertown, Massachusetts 02172 USA
CTS	CTS Corporation 1142 West Beardsley Avenue Elkart, Indiana 46514 USA
Ducati	Ducati Distributor Consolidated Distributors, Inc. 129 Hudson Street New York, New York 10013 USA
GE	General Electric Company Oak Brook Executive Plaza Oak Brook, Illinois 60521 USA
General Radio	General Radio Company 300 Baker Avenue West Concord, Massachusetts 01781 USA
IRC	International Resistor Corporation Division of TRW 401 North Broad Street Philadelphia, Pennsylvania 19108 USA
Littelfuse	Littelfuse, Inc. 800 East Northwest Highway Des Plaines, Illinois 60016 USA
Microtran	Microtran Company, Inc. 145 East Mineola Avenue Valley Stream, New York 11582 USA
PEM	PEM Machine Tool Company, Inc. 39A Myrtle Street Cranford, New Jersey 07016 USA
RCA	RCA Electronic Components 415 South Fifth Street Harrison, New Jersey 07029 USA

Schauer	Schauer Manufacturing Corporation 4516 Alpine Avenue Cincinnati, Ohio 45242 USA
Siemens	Siemens America, Inc. Telecommunications Division 350 Fifth Avenue New York, New York 10001 USA
Solitron	Solitron Devices, Inc. Transistor Division 1177 Blue Heron Road Riviera Beach, Florida 33404 USA
Sprague	Sprague Electric Company 125 Marshall Street North Adams, Massachusetts 02147 USA
Switchcraft	Switchcraft, Inc. 5555 North Elston Avenue Chicago, Illinois 60630 USA
Varo	Varo, Inc. Semiconductor Division 1000 North Shiloh Road Garland, Texas 75041 USA
VECO	Victory Engineering Corporation 128 Victory Road Springfield, New Jersey 07081 USA

8.0 SUPPLEMENTARY DATA

8.1 Guarantee

Bowmar/ALI, Inc. guarantees to the original purchaser that this instrument is in accordance with applicable specifications. Any deviation from these specifications and any defects in workmanship or materials will be corrected by Bowmar/ALI, Inc., provided the instrument has been properly used under normal operating conditions. This guarantee is effective for one year from date of shipment except for failure of or attributable to tubes, fuses, batteries, or semiconductors after ninety days from date of shipment. Bowmar/ALI, Inc. will be the sole judge of the validity of all claims.

All returns made under this guarantee must be authorized in writing by Bowmar/ALI, Inc. Such authorization will be given only upon receipt of information concerning type, serial number, and the defect claimed. Return shipments must be made prepaid except returns authorized within thirty days from date of shipment, in which case Railway Express Collect will be authorized. All rework done under this guarantee will be re-shipped prepaid from our plant.

Bowmar/ALI, Inc. will not be responsible for, nor assume any expense or liability for, damage of loss in shipment, loss of profit, or any other damages or claims for which provisions are not specifically made herein.

8.2 Material Damaged in Shipment

Upon receipt of the instrument, do not unpack if the packing case shows evidence of damage; upon unpacking, do not discard any of the packing if damage is found which appears to have been caused by shipment. Immediately notify the local office of the carrier and request that the damage be inspected; also, notify Bowmar/ALI, Inc. of the model number, serial number, carrier's number, date received, and any other pertinent information so that we may contact the local carrier office and facilitate a speedy settlement of any claim.

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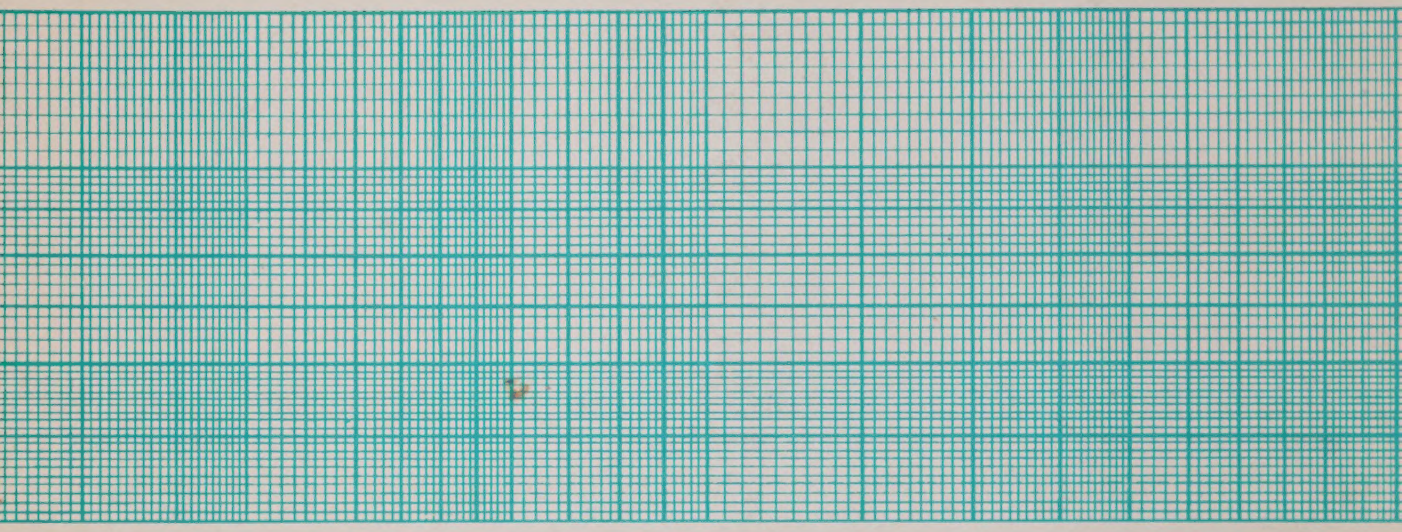

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